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Title:

The Fire Resistance Performance of Steel 'I' and 'H' Section Beams and Columns Protected with CONTEGO Passive Fire Barrier Latex Intumescent in Accordance with BS 476: Part 21: 1987: Analysis at Various Design Temperatures.

WF Report No:

348293 Issue 2

Prepared for:

Contego International Inc.

1013 Arthur Street,
Rochester,
Indiana
United States of America,
IN 46975

Date:

26th January 2016

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Executive Summary

Objective To provide an assessment of the ability of an intumescent coating system known as CONTEGO Passive Fire Barrier Latex Intumescent to fire protect structural steel I/H-section Beams and Columns in accordance with BS 476: Part 21: 1987 for design temperatures in the range 350°C to 750°C and fire resistance periods up to 120 minutes.

Report Sponsor **Contego International Inc.**

Address 1013 Arthur Street, Rochester, Indiana, United States of America, IN 46975

Summary of Conclusions An assessment of the ability of an intumescent coating system known as CONTEGO Passive Fire Barrier Latex Intumescent to protect structural steel I/H-section Beams and Columns in accordance with BS 476: Part 21: 1987 for periods up to 120 minutes.

The input data for the assessment was generated from tests on sections subjected to the heating conditions in accordance with BS EN 13381-8: 2013.

Because the conditions of furnace temperature which are achieved during the test in accordance to BS EN 13381-8: 2013 represent a more severe exposure to the test specimens, it is considered to be conservative to use the test results for the purpose of this assessment.

The report considers the ability of CONTEGO Passive Fire Barrier Latex Intumescent to fire protect structural steel I/H-section Beams and Columns for design temperatures in the range of 350°C to 750°C and fire resistance periods up to 120 minutes in the light of additional test data.

The assessment utilises a graphical method plotting inverse section factor against time to reach the specified steel temperature for a range of protection thickness.

Appendix 1 shows the test data used in the analyses.

Annexes A and B show the analyses and the results for I/H-section Beams and Columns.

Valid until 1st February 2021

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Introduction

This report presents an assessment of the ability of an intumescent coating system known as CONTEGO Passive Fire Barrier Latex Intumescent to protect structural steel I/H-section Beams and Columns in accordance with BS 476: Part 21: 1987 for periods up to 120 minutes in the light of additional test data.

The input data for the assessment was generated from tests on sections subjected to the heating conditions in accordance with BS EN 13381-8: 2013.

Because the conditions of furnace temperature which are achieved during the test in accordance to BS EN 13381-8: 2013 represent a more severe exposure to the test specimens, it is considered to be conservative to use the test results for the purpose of this assessment.

This report sets out three criteria for the assessment to be deemed satisfactory. These criteria for acceptability are:

- (a) For each short section the predicted time to reach each design temperature shall not exceed the time for the corrected temperature to reach the design temperature by more than 15%.
- (b) The mean value of all percentage differences in time shall be less than zero.
- (c) A maximum of 30% of individual values of all percentage differences in time shall be more than zero.

The assessment for beams with 3-sided protection refers to a concrete slab in intimate contact with the top flange.

FTSG

The data referred to in the supporting data section has been considered for the purpose of this appraisal which has been prepared in accordance with the Fire Test Study Group Resolution No. 82: 2001.

Assumptions

Steel preparation It is assumed that the steel sections will be shot-blast cleaned and primed with a similar paint in a similar manner to that used for the sections tested under the test references given in the original report.

Primer

This report assumes that nominal thickness of the primer paint will be similar to that for the tested sections.

Test Data

Data from the loaded tests and the tests on the tall column

The following tests were carried out on loaded beams and tall column:

Loaded I-section Beams

| Test Reference | Section Reference | Section Size mm×mm×kg/m | Actual Section Factor m ⁻¹ | Coating Thickness mm | Load Bearing Capacity minutes |
|----------------|--------------------|-------------------------|---------------------------------------|----------------------|-------------------------------|
| WF No. 352790 | LB1 _{min} | 406 x 178 x 67 | 162 | 0.306 | 26 |
| WF No. 354436 | LB1 _{max} | 406 x 178 x 67 | 167.9 | 3.551 | 111 |

Tall H-section Column

| Test Reference | Section Reference | Section Size mm×mm×kg/m | Actual Section Factor m ⁻¹ | Coating Thickness mm | Time to Reach 550°C minutes |
|----------------|-------------------|-------------------------|---------------------------------------|----------------------|-----------------------------|
| WF No. 343254 | TC1 | 203x203x60 | 173.9 | 4.224 | 108.5 |

The specimens were subjected to the heating conditions of BS EN 13381-8: 2013. Because the conditions of furnace temperature which are achieved during the test in accordance to BS EN 13381-8: 2013 represent a more severe exposure, it is considered to be conservative to use the test results for the purpose of this assessment.

The tests referred to above demonstrate the ability of the coating to remain attached to a deflecting section and free from slumping at elevated temperatures. The beam sections were loaded to produce the maximum permissible stress for the steel grade.

I/H-section Beams

Typically if the loaded beam achieves within 10% of the maximum required, it is considered acceptable to derive specifications for up to the maximum i.e. 120 minutes in this case.

The loaded beam from the test WF No. 354436 with the maximum protection thickness achieved a minimum fire resistance performance of 111 minutes therefore, it is acceptable to derive specifications for up to 120 minutes.

I/H-section Columns

For the assessment of H-section columns a critical steel temperature of 550°C is considered to be appropriate (the Yellow Book guidelines).

As the tall column from the test WF No. 343254 with the maximum protection thickness achieved a minimum fire resistance performance of 108 minutes therefore, it is acceptable to derive specifications for up to 120 minutes.

Data correction

Data correction was carried out by comparing the time for the loaded beams or tall column to reach each of the specified temperatures with those for the equivalent short reference sections.

It is unlikely that the loaded beam or tall column and its equivalent short reference sections will have identical section factors and protection thickness. Therefore the time for the short beam is adjusted to the same section factor and thickness as the loaded beam or tall column.

Where a correction factor was >1.0, a correction factor of 1 was adopted.

The calculation of the correction factors for the specified steel temperatures is given in Appendix 1.

Analysis Methods

I/H-sections

For this report the thickness of the protection material for I/H-section beams and I/H-section columns was determined by multi-temperature analysis.

The relevant temperature data was derived from short columns therefore, the thermal analysis can be used for both beams (3 sided protection) and columns (4 sided protection). The data used in the analysis across the temperature range of 350°C to 750°C, including those given above, is summarised in Appendix 1.

The details of each specimen, i.e. the section factor (the ratio of the heated perimeter to cross-sectional area – A/V), the protection thickness and duration of heating required for the sections to reach an appropriate design temperature were used as input data for the analysis.

The fire resistance of a protected steel section can be approximated as follows over a limited range of values:

$FR \propto A/V$ at a constant protection thickness or

$d \propto A/V$ at a constant fire resistance period

where;

FR - Fire resistance

V - Cross-sectional area

A - Heater perimeter of section

d - Thickness of protection material

The required thickness of protection for a given steel section for a particular fire resistance period is therefore assessed by means of a graphical plot of inverse section factor (V/A) against the time for the section to reach the critical steel temperature.

Assessed Performance

General

Experience shows that data from fire resistance tests on steel sections protected with intumescent coatings, when presented graphically as inverse section factor against time to reach a particular steel temperature, tend to show a curved relationship.

This report adopts a conservative approach when drawing plots by generally drawing straight lines through the data points or by giving equal validity for corresponding data points.

Graphs

The graphs in Annexes A and B represent specified steel temperatures as indicated in this report.

Intercepts

Although some intercepts show high section factors these have only been used to determine the appropriate thickness for the maximum section factor for each section type.

Analysis and Results

Annexes A and B show the graphical plots for the various steel temperatures, the intercepts from the graphs and tables showing the results for I/H-section Beams and Columns respectively.

Scope of Performance

In line with current UK assessment principles it is permitted to extend the scope of the assessment with respect to protection thickness and section factor by approximately 10%.

Permitted extensions

These limitations applied to the analysis are as follows:

I/H-section Beams

| Permitted Extension for Protection Thickness | | | |
|--|-----------|----------------------|----------------------|
| I/H-Section Beams | Actual mm | Maximum Permitted mm | Minimum Permitted mm |
| LB1min | 0.306 | - | 0.275 |
| LB1max | 3.551 | 3.906 | - |

| Permitted Extension for Section Factor | | | |
|--|-----------------|----------------------------|----------------------------|
| I/H-Section Beams | Actual m^{-1} | Maximum Permitted m^{-1} | Minimum Permitted m^{-1} |
| SC4 | 95 | - | 86 |
| SC10 | 334 | 368 | - |

I/H-section Columns

| Permitted Extension for Protection Thickness | | | |
|--|-----------|----------------------|----------------------|
| I/H-Section Columns | Actual mm | Maximum Permitted mm | Minimum Permitted mm |
| SC2 | 0.289 | - | 0.260 |
| TC1 | 4.224 | 4.646 | - |

| Permitted Extension for Section Factor | | | |
|--|-----------------|----------------------------|----------------------------|
| I/H-Section Columns | Actual m^{-1} | Maximum Permitted m^{-1} | Minimum Permitted m^{-1} |
| SC4 | 95 | - | 86 |
| SC10 | 334 | 367 | - |

Four sided beams

The results of the assessment for columns can be applied to beams exposed on all four sides up to the maximum dry film thickness of 3.906mm.

The result of the analysis of the data for I/H-section beams supporting concrete slab as given in WF Nos. 352790 and 354436 is also applicable to beams with web depth up to 610mm.

Design temperatures

Specific results referred to in the Annexes at temperatures of 620°C (I-section beams) and 550°C (H-section columns) relate to steel sections subjected to the maximum design loads in accordance with BS 449: Part 2.

Limits of applicability

The method of protection should be as described in the appropriate test report.

Conclusions

An assessment of the ability of an intumescent coating system known as CONTEGO Passive Fire Barrier Latex Intumescent to fire protect structural steel I/H-section Beams and Columns in accordance with BS 476: Part 21: 1987 for design temperatures in the range 350°C to 750°C and fire resistance periods up to 120 minutes has been undertaken.

The assessment method adopted for this report uses a graphical approach plotting inverse section factor against time to reach a specified steel temperature for a range of protection thickness. This method is commonly used in the UK for assessing the ability of reactive intumescent protection systems to fire protect structural steel.

This report considers steel design temperatures in the range 350°C to 750°C and fire resistance periods up to 120 minutes.

Appendix 1 shows the test data used in the analyses.

Annexes A and B show the graphical plots for the various steel temperatures, the intercepts from the graphs and tables showing the results for I/H-section Beams and Columns respectively.

Validity

This assessment is issued on the basis of test data and information available at the time of issue.

If contradictory evidence becomes available to **Exova Warringtonfire** the assessment will be unconditionally withdrawn and Contego International Inc. will be notified in writing. Similarly the assessment is invalidated if the assessed construction is subsequently tested because actual test data is deemed to take precedence over an expressed opinion.

The assessment is valid initially for a period of five years i.e. until 1st February 2021 after which time it is recommended that it be returned for re-appraisal.

The appraisal is only valid provided that no other modifications are made to the tested construction other than those described in this report.

Summary of Supporting Data

WF Nos. 343253, 343254, 344018, 354436, 352790 and 352791 Reports on fire resistance tests in accordance with EN 13381-8: 2013 carried out on loaded sections and a number of unloaded 'I' and 'H' sections subjected to the heating conditions specified in this standard.

The appropriate details of the test sections are summarised in the body of this report.

The tests were sponsored by Contego International Inc.

Declaration by Contego International Inc.

We the undersigned confirm that we have read and complied with the obligations placed on us by the UK Fire Test Study Group Resolution No. 82: 2001.

We confirm that the component or element of structure, which is the subject of this assessment, has not to our knowledge been subjected to a fire test to the Standard against which the assessment is being made.

We agree to withdraw this assessment from circulation should the component or element of structure be the subject of a fire test to the Standard against which this assessment is being made.

We are not aware of any information that could adversely affect the conclusions of this assessment.

If we subsequently become aware of any such information we agree to cease using the assessment and ask **Exova Warringtonfire** to withdraw the assessment.

Signed:



John M. Schwartz* - Director, International Operations

For and on behalf of: Contego International Inc.

Signatories



Responsible Officer
D Podolski* - Certification Engineer



Approved
Jifeng Yuan * – Chief Engineer

* For and on behalf of **Exova Warringtonfire**.

Report Issued: 26th January 2016

2nd Issue presents fire resistance periods up to 120 minutes
and additional design temperatures - **3rd February 2016**

The assessment report is not valid unless it incorporates the declaration duly signed by the applicant.

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Appendix 1

Appendix 1 Test Data: I/H-section Beams

I/H-section Beams Data

| Section | Section Factor m ⁻¹ | Thickness mm | | Design Temperature | | | | | | | | | | |
|----------------|--------------------------------|--------------|----------------|--------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | | | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 620°C | 650°C | 700°C | 750°C | |
| Section SC7 | 262 | 1.747 | Factor | 1.000 | 0.995 | 0.997 | 0.995 | 0.995 | 0.995 | 0.995 | 0.995 | 0.995 | 0.995 | |
| | | | Actual Time | 42.8 | 51.8 | 60.5 | 69.1 | 78.1 | 87.5 | 91.5 | 97.6 | 108.3 | 119.5 | |
| | | | Corrected Time | 42.7 | 51.5 | 60.3 | 68.7 | 77.6 | 87.0 | 91.0 | 97.0 | 107.7 | 118.8 | |
| Section SC2 | 174 | 2.319 | Factor | 1.000 | 0.997 | 0.998 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 |
| | | | Actual Time | 62.5 | 74.5 | 85.2 | 96.1 | 107.0 | 118.7 | 123.5 | 131.0 | 144.0 | 155.3 | 155.3 |
| | | | Corrected Time | 62.4 | 74.2 | 85.0 | 95.7 | 106.6 | 118.2 | 123.0 | 130.5 | 143.4 | 154.7 | 154.7 |
| Section SC5 | 95 | 2.345 | Factor | 1.000 | 0.997 | 0.998 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 |
| | | | Actual Time | 84.0 | 98.7 | 112.7 | 126.7 | 141.5 | 155.0 | 160.0 | 163.3 | 167.0 | 171.5 | 171.5 |
| | | | Corrected Time | 83.9 | 98.4 | 112.4 | 126.2 | 141.0 | 154.4 | 159.4 | 162.7 | 166.4 | 170.8 | 170.8 |
| Section SC4 | 95 | 1.696 | Factor | 1.000 | 0.995 | 0.997 | 0.995 | 0.995 | 0.995 | 0.995 | 0.995 | 0.995 | 0.995 | 0.995 |
| | | | Actual Time | 59.2 | 72.7 | 85.5 | 98.2 | 111.0 | 124.2 | 129.7 | 138.5 | 152.6 | 166.0 | 166.0 |
| | | | Corrected Time | 59.1 | 72.3 | 85.2 | 97.6 | 110.3 | 123.5 | 128.9 | 137.7 | 151.7 | 165.0 | 165.0 |
| Section SC8 | 262 | 2.333 | Factor | 1.000 | 0.997 | 0.998 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 |
| | | | Actual Time | 50.0 | 59.3 | 68.1 | 77.2 | 86.8 | 97.1 | 101.3 | 107.7 | 119.0 | 129.0 | 129.0 |
| | | | Corrected Time | 49.9 | 59.1 | 67.9 | 76.9 | 86.4 | 96.7 | 100.9 | 107.3 | 118.5 | 128.5 | 128.5 |
| Section SC9 | 262 | 4.083 | Factor | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| | | | Actual Time | 64.5 | 73.1 | 79.1 | 84.6 | 90.7 | 97.6 | 100.6 | 105.5 | 114.0 | 122.5 | 122.5 |
| | | | Corrected Time | 64.5 | 73.1 | 79.1 | 84.6 | 90.7 | 97.6 | 100.6 | 105.5 | 114.0 | 122.5 | 122.5 |
| Section SC10 | 334 | 1.692 | Factor | 1.000 | 0.995 | 0.997 | 0.995 | 0.995 | 0.995 | 0.995 | 0.995 | 0.995 | 0.995 | 0.995 |
| | | | Actual Time | 36.1 | 44.6 | 52.3 | 60.3 | 68.7 | 77.8 | 81.5 | 87.3 | 97.0 | 107.6 | 107.6 |
| | | | Corrected Time | 36.0 | 44.3 | 52.1 | 59.9 | 68.3 | 77.3 | 81.0 | 86.8 | 96.4 | 107.0 | 107.0 |
| Section SC11 | 334 | 2.305 | Factor | 1.000 | 0.997 | 0.998 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 | 0.996 |
| | | | Actual Time | 45.5 | 54.6 | 62.3 | 70.0 | 78.1 | 86.6 | 90.2 | 95.8 | 105.1 | 115.0 | 115.0 |
| | | | Corrected Time | 45.4 | 54.4 | 62.1 | 69.7 | 77.8 | 86.2 | 89.8 | 95.4 | 104.7 | 114.5 | 114.5 |
| Section SC12 | 334 | 3.956 | Factor | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| | | | Actual Time | 64.3 | 73.8 | 81.8 | 89.6 | 97.6 | 106.3 | 110.0 | 116.0 | 127.0 | 138.1 | 138.1 |
| | | | Corrected Time | 64.3 | 73.8 | 81.8 | 89.6 | 97.6 | 106.3 | 110.0 | 116.0 | 127.0 | 138.1 | 138.1 |
| Section SC6 | 250 | 0.598 | Factor | 1.000 | 0.993 | 0.995 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 |
| | | | Actual Time | 23.5 | 31.2 | 38.1 | 44.7 | 51.2 | 57.3 | 59.8 | 63.5 | 69.7 | 77.3 | 77.3 |
| | | | Corrected Time | 23.4 | 30.9 | 37.9 | 44.3 | 50.7 | 56.8 | 59.2 | 62.9 | 69.0 | 76.6 | 76.6 |
| Section SC3 | 97 | 0.627 | Factor | 1.000 | 0.993 | 0.995 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 |
| | | | Actual Time | 31.2 | 40.7 | 50.0 | 58.6 | 66.8 | 74.5 | 77.6 | 82.1 | 90.2 | 99.6 | 99.6 |
| | | | Corrected Time | 31.1 | 40.4 | 49.7 | 58.0 | 66.2 | 73.8 | 76.9 | 81.3 | 89.4 | 98.7 | 98.7 |
| Section SC1 | 172 | 0.637 | Factor | 1.000 | 0.993 | 0.995 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 |
| | | | Actual Time | 24.2 | 31.8 | 39.2 | 46.5 | 53.7 | 60.7 | 63.5 | 67.5 | 74.6 | 83.0 | 83.0 |
| | | | Corrected Time | 24.1 | 31.5 | 39.0 | 46.1 | 53.2 | 60.1 | 62.9 | 66.9 | 73.9 | 82.2 | 82.2 |
| Section TC1 | 174 | 4.224 | Factor | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| | | | Actual Time | 73.7 | 85.3 | 93.8 | 101.1 | 108.8 | 116.6 | 119.6 | 123.8 | 128.3 | 129.9 | 129.9 |
| | | | Corrected Time | 73.7 | 85.3 | 93.8 | 101.1 | 108.8 | 116.6 | 119.6 | 123.8 | 128.3 | 129.9 | 129.9 |
| Section SC1min | 96 | 0.289 | Factor | 1.000 | 0.992 | 0.995 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 |
| | | | Actual Time | 20.5 | 26.0 | 31.1 | 35.8 | 40.0 | 44.2 | 45.9 | 48.7 | 54.0 | 61.6 | 61.6 |
| | | | Corrected Time | 20.4 | 25.7 | 30.9 | 35.4 | 39.6 | 43.7 | 45.4 | 48.2 | 53.4 | 61.0 | 61.0 |
| Section SC2min | 170 | 0.289 | Factor | 1.000 | 0.992 | 0.995 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 |
| | | | Actual Time | 14.4 | 18.8 | 23.1 | 27.3 | 31.8 | 36.6 | 38.6 | 41.5 | 46.2 | 52.1 | 52.1 |
| | | | Corrected Time | 14.3 | 18.6 | 22.9 | 27.0 | 31.4 | 36.2 | 38.2 | 41.1 | 45.7 | 51.6 | 51.6 |
| Section SC3min | 254 | 0.309 | Factor | 1.000 | 0.992 | 0.995 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 | 0.991 |
| | | | Actual Time | 10.4 | 14.3 | 18.4 | 22.0 | 25.8 | 30.0 | 31.8 | 34.6 | 39.5 | 44.8 | 44.8 |
| | | | Corrected Time | 10.3 | 14.1 | 18.3 | 21.7 | 25.5 | 29.7 | 31.4 | 34.2 | 39.1 | 44.3 | 44.3 |

I/H-section Beams Correction

| Section | LB1min | RB1min | |
|-----------------------------|--------|--------|--|
| Section Factor (m^{-1}) | 162.0 | 161.9 | |
| Thickness (mm) | 0.306 | 0.299 | |

| Design temperature | Time to reach temperature | | RB1min Corrected time | Factor |
|--------------------|---------------------------|--------|-----------------------|--------|
| | LB1min | RB1min | | |
| 350 | 13.7 | 13.4 | 13.7 | 1.000 |
| 400 | 18.2 | 18.0 | 18.4 | 0.992 |
| 450 | 22.8 | 22.4 | 22.9 | 0.995 |
| 500 | 27.3 | 26.8 | 27.4 | 0.991 |
| 550 | 32.1 | 31.5 | 32.2 | 0.991 |
| 600 | 37.1 | 36.4 | 37.3 | 0.991 |
| 620 | 39.1 | 38.2 | 39.1 | 0.991 |
| 650 | 42.0 | 41.0 | 41.9 | 0.991 |
| 700 | 47.4 | 45.2 | 46.3 | 0.991 |
| 750 | 52.1 | 49.9 | 51.1 | 0.991 |

| Section | LB1max | RB1max | |
|-----------------------------|--------|--------|--|
| Section Factor (m^{-1}) | 167.9 | 167.2 | |
| Thickness (mm) | 3.551 | 3.398 | |

| Design temperature | Time to reach temperature | | RB1max Corrected time | Factor |
|--------------------|---------------------------|--------|-----------------------|--------|
| | LB1max | RB1max | | |
| 350 | 72.6 | 65.3 | 68.0 | 1.000 |
| 400 | 84.9 | 76.4 | 79.5 | 1.000 |
| 450 | 97.1 | 87.0 | 90.6 | 1.000 |
| 500 | 109.5 | 97.8 | 101.7 | 1.000 |
| 550 | 122.3 | 108.6 | 113.0 | 1.000 |
| 600 | 136.5 | 119.5 | 124.4 | 1.000 |
| 620 | 142.3 | 124.2 | 129.3 | 1.000 |
| 650 | 151.6 | 131.3 | 136.6 | 1.000 |
| 700 | 170.0 | 143.9 | 149.7 | 1.000 |
| 750 | 186.1 | 159.3 | 165.8 | 1.000 |

Appendix 2 Test Data: I/H-section Columns

I/H-section Columns Data

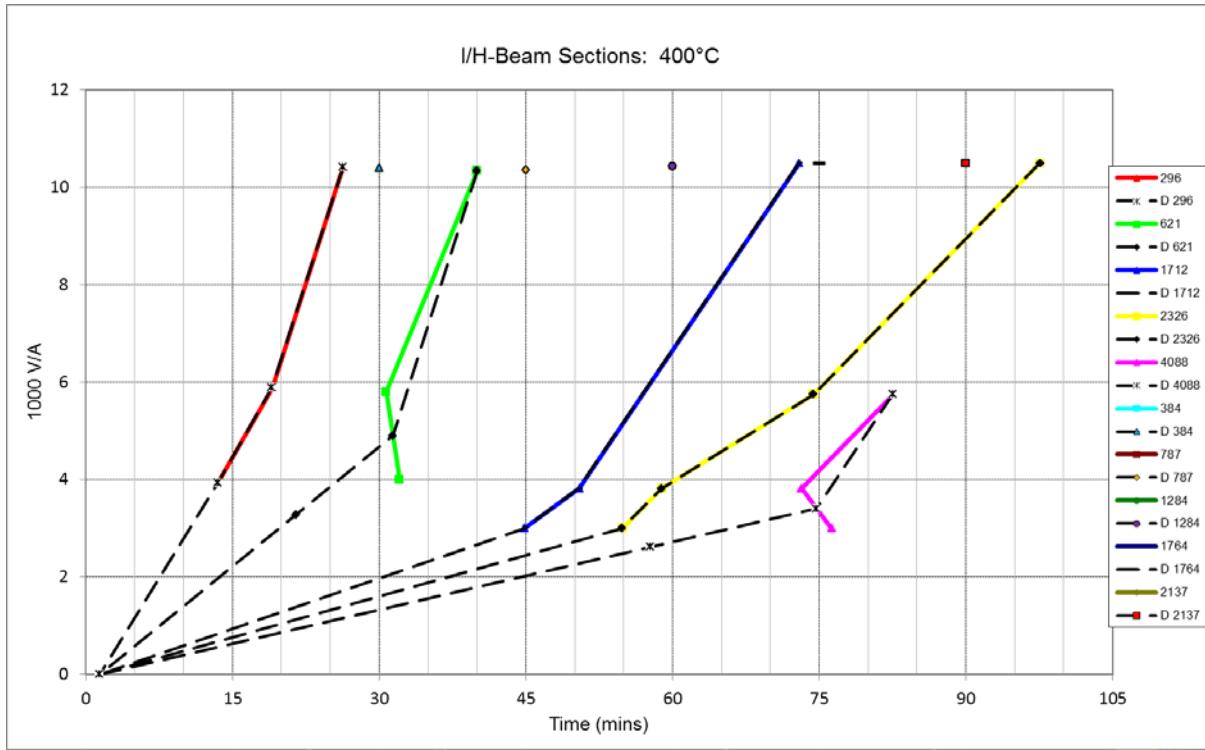
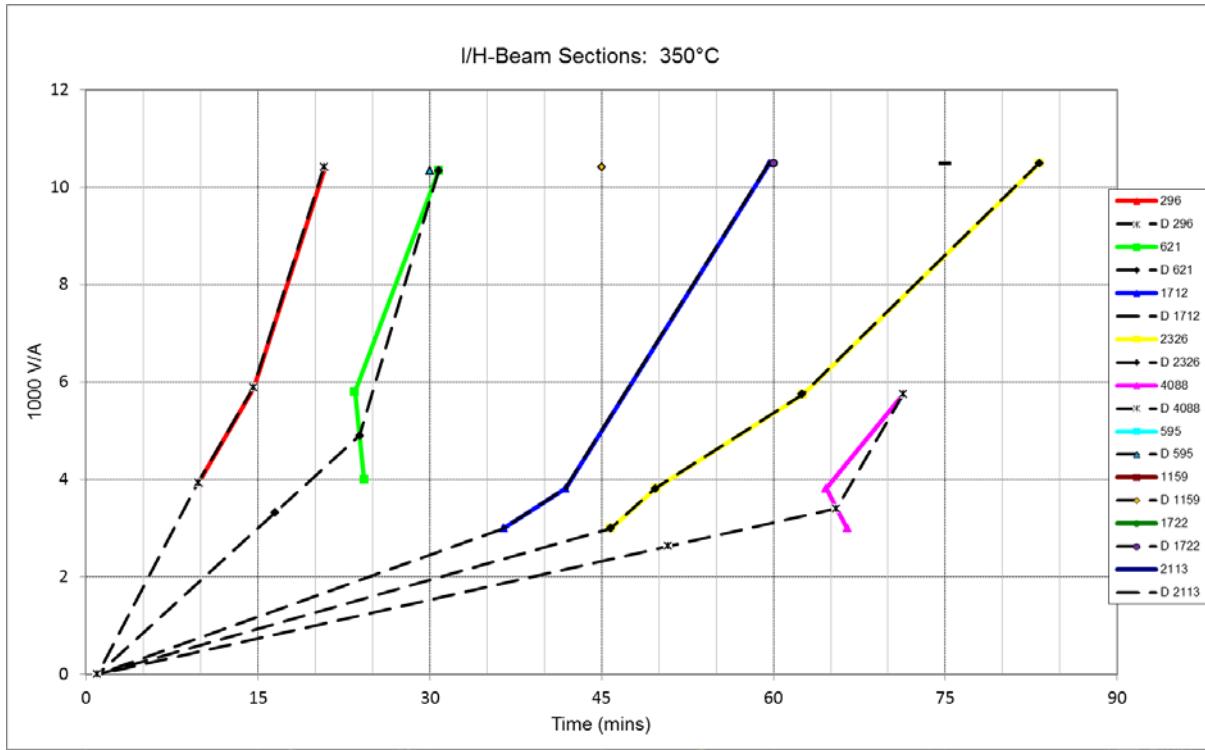
| Section | Section Factor m ⁻¹ | Thickness mm | | Design Temperature | | | | | | | | |
|----------------|--------------------------------|--------------|----------------|--------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | | | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 650°C | 700°C | 750°C |
| Section SC7 | 262 | 1.747 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 42.8 | 51.8 | 60.4 | 69.2 | 78.1 | 87.5 | 97.6 | 108.3 | 119.5 |
| | | | Corrected Time | 41.2 | 50.3 | 58.9 | 67.3 | 75.7 | 84.4 | 92.9 | 99.6 | 105.2 |
| Section SC2 | 174 | 2.319 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 62.5 | 74.5 | 85.3 | 96.1 | 107.0 | 118.7 | 130.9 | 143.9 | 155.3 |
| | | | Corrected Time | 60.2 | 72.4 | 83.3 | 93.5 | 103.8 | 114.5 | 124.6 | 132.4 | 136.7 |
| Section SC5 | 95 | 2.345 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 84.0 | 98.7 | 112.8 | 126.7 | 141.5 | 155.0 | 163.3 | 167.0 | 171.4 |
| | | | Corrected Time | 80.9 | 95.9 | 110.1 | 123.3 | 137.2 | 149.6 | 155.5 | 153.6 | 150.9 |
| Section SC4 | 95 | 1.696 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 59.3 | 72.7 | 85.5 | 98.2 | 110.9 | 124.2 | 138.5 | 152.6 | 166.0 |
| | | | Corrected Time | 57.1 | 70.6 | 83.5 | 95.6 | 107.6 | 119.8 | 131.9 | 140.4 | 146.1 |
| Section SC8 | 262 | 2.333 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 50.0 | 59.3 | 68.1 | 77.2 | 86.8 | 97.1 | 107.8 | 118.9 | 128.9 |
| | | | Corrected Time | 48.1 | 57.6 | 66.5 | 75.1 | 84.2 | 93.7 | 102.6 | 109.4 | 113.5 |
| Section SC9 | 262 | 4.083 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 64.5 | 73.1 | 79.1 | 84.6 | 90.7 | 97.6 | 105.4 | 114.0 | 122.4 |
| | | | Corrected Time | 62.1 | 71.0 | 77.2 | 82.3 | 88.0 | 94.2 | 100.3 | 104.8 | 107.7 |
| Section SC10 | 334 | 1.692 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 36.1 | 44.7 | 52.3 | 60.2 | 68.7 | 77.7 | 87.2 | 97.1 | 107.6 |
| | | | Corrected Time | 34.7 | 43.4 | 51.0 | 58.6 | 66.6 | 74.9 | 83.0 | 89.3 | 94.7 |
| Section SC11 | 334 | 2.305 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 45.5 | 54.6 | 62.3 | 70.0 | 78.1 | 86.6 | 95.8 | 105.1 | 114.9 |
| | | | Corrected Time | 43.8 | 53.0 | 60.8 | 68.1 | 75.7 | 83.5 | 91.2 | 96.7 | 101.1 |
| Section SC12 | 334 | 3.956 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 64.3 | 73.8 | 81.8 | 89.6 | 97.6 | 106.2 | 115.9 | 126.9 | 138.1 |
| | | | Corrected Time | 61.9 | 71.7 | 79.9 | 87.2 | 94.6 | 102.5 | 110.3 | 116.7 | 121.6 |
| Section SC6 | 250 | 0.598 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 23.4 | 31.2 | 38.1 | 44.7 | 51.2 | 57.3 | 63.4 | 69.7 | 77.3 |
| | | | Corrected Time | 22.5 | 30.3 | 37.2 | 43.5 | 49.6 | 55.3 | 60.3 | 64.1 | 68.0 |
| Section SC3 | 97 | 0.627 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 31.2 | 40.7 | 49.9 | 58.6 | 66.8 | 74.5 | 82.2 | 90.2 | 99.6 |
| | | | Corrected Time | 30.0 | 39.5 | 48.7 | 57.0 | 64.8 | 71.9 | 78.2 | 82.9 | 87.7 |
| Section SC1 | 172 | 0.637 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 24.2 | 31.9 | 39.2 | 46.5 | 53.7 | 60.7 | 67.5 | 74.6 | 83.0 |
| | | | Corrected Time | 23.3 | 31.0 | 38.2 | 45.2 | 52.1 | 58.5 | 64.2 | 68.6 | 73.0 |
| Section TC1 | 174 | 4.224 | Factor | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| | | | Actual Time | 73.7 | 85.3 | 93.8 | 101.2 | 108.8 | 116.6 | 123.8 | 128.3 | 129.9 |
| | | | Corrected Time | 73.7 | 85.3 | 93.8 | 101.2 | 108.8 | 116.6 | 123.8 | 128.3 | 129.9 |
| Section SC1min | 96 | 0.289 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 20.6 | 26.0 | 31.1 | 35.8 | 40.0 | 44.2 | 48.7 | 54.0 | 61.6 |
| | | | Corrected Time | 19.8 | 25.2 | 30.3 | 34.8 | 38.8 | 42.6 | 46.3 | 49.6 | 54.2 |
| Section SC2min | 170 | 0.289 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 14.4 | 18.8 | 23.1 | 27.3 | 31.8 | 36.6 | 41.5 | 46.2 | 52.1 |
| | | | Corrected Time | 13.8 | 18.2 | 22.5 | 26.5 | 30.8 | 35.3 | 39.5 | 42.5 | 45.8 |
| Section SC3min | 254 | 0.309 | Factor | 0.963 | 0.972 | 0.977 | 0.974 | 0.970 | 0.965 | 0.952 | 0.920 | 0.881 |
| | | | Actual Time | 10.4 | 14.3 | 18.4 | 22.0 | 25.8 | 30.0 | 34.6 | 39.5 | 44.9 |
| | | | Corrected Time | 10.0 | 13.8 | 17.9 | 21.4 | 25.0 | 28.9 | 32.9 | 36.3 | 39.5 |

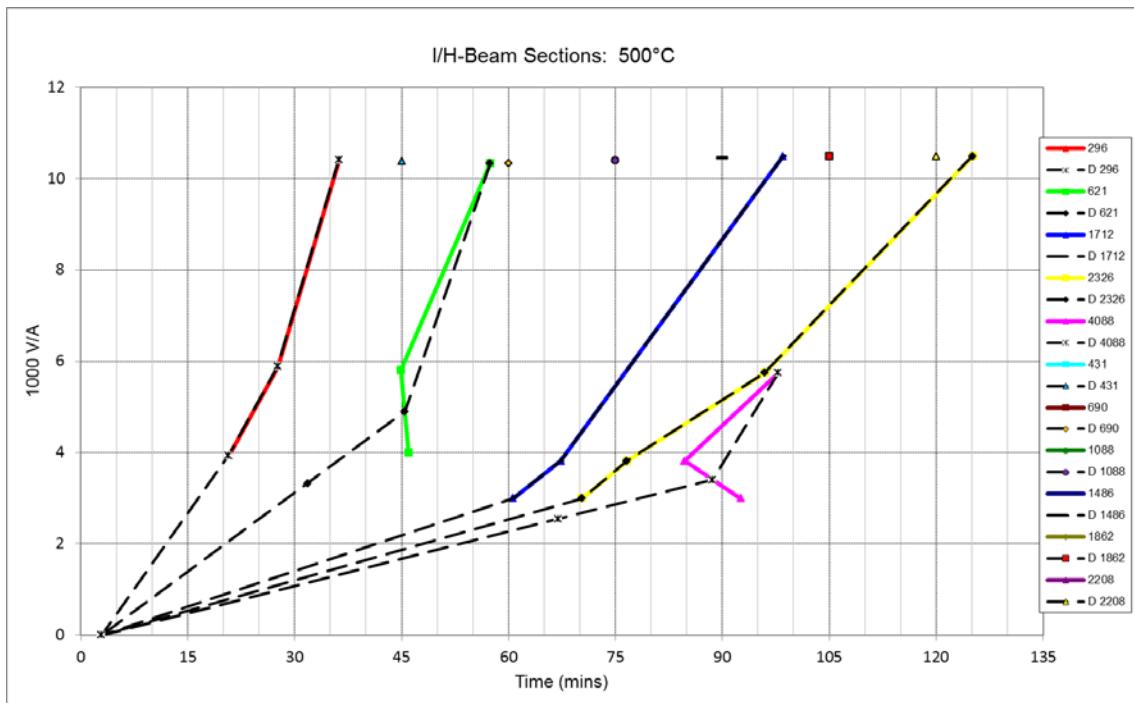
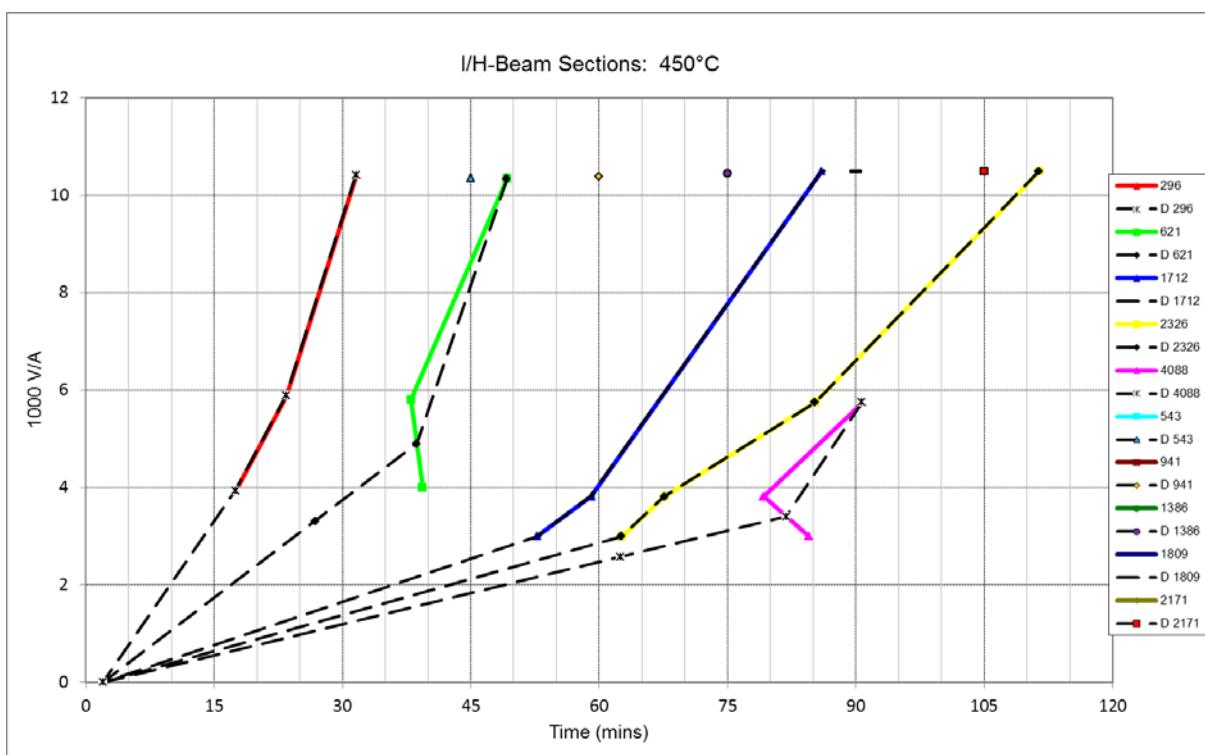
I/H-section Columns Correction

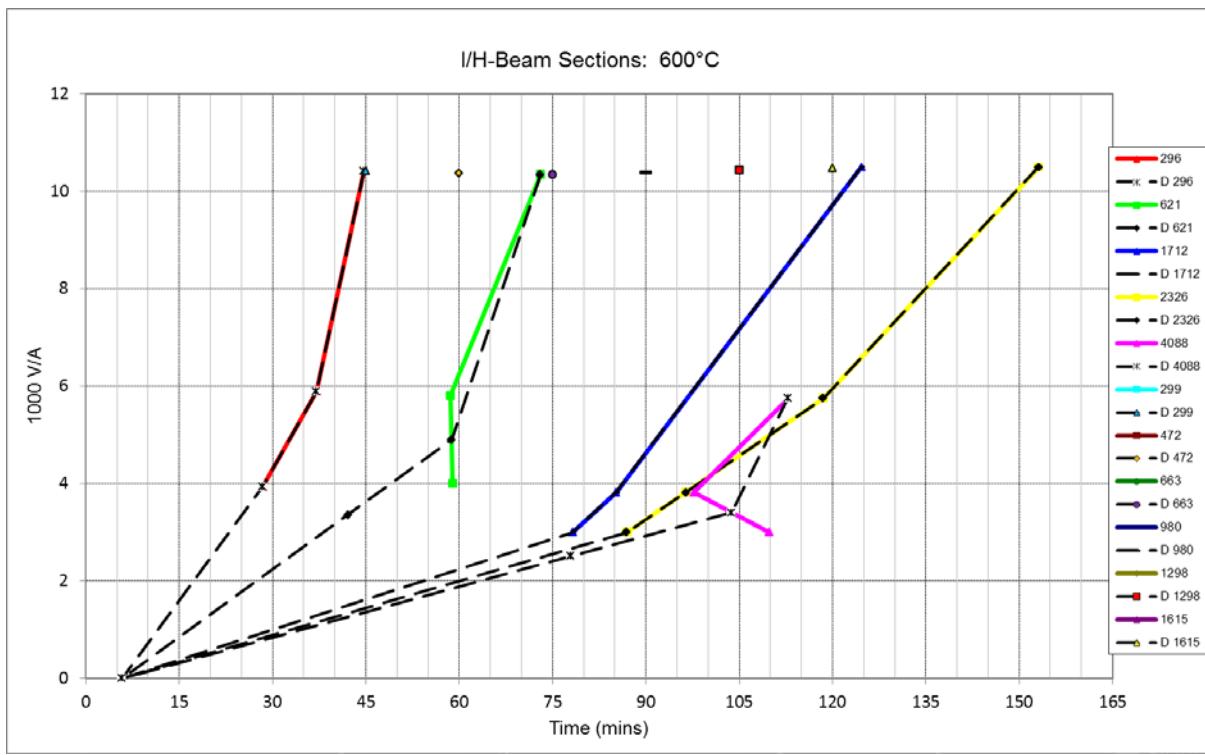
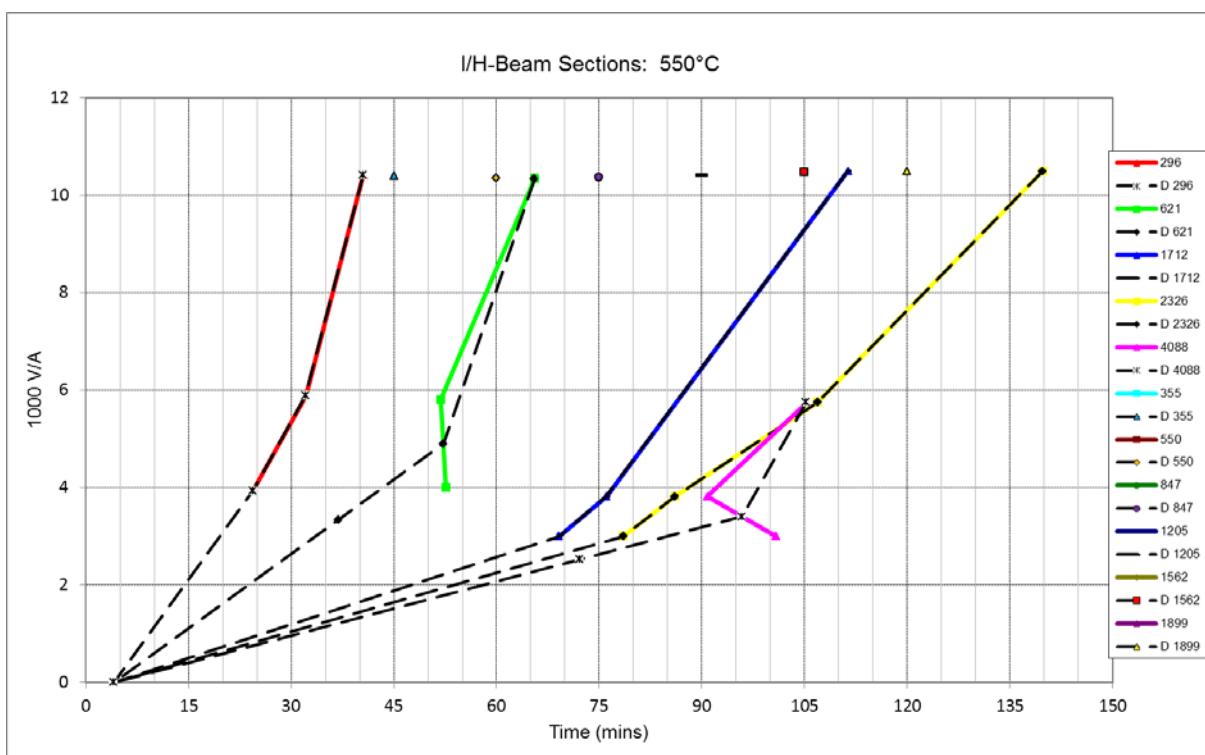
| Section | TC1 | RC1 | | |
|--------------------|---------------------------|-------|--------------------|--------|
| Section Factor m-1 | 173.9 | 173.9 | | |
| Thickness (mm) | 4.224 | 4.184 | | |
| <hr/> | | | | |
| Design temperature | Time to reach temperature | | RC1 Corrected time | Factor |
| | TC1 | RC1 | | |
| 350 | 73.8 | 75.8 | 76.6 | 0.963 |
| 400 | 85.3 | 86.9 | 87.8 | 0.972 |
| 450 | 93.9 | 95.2 | 96.1 | 0.977 |
| 500 | 101.2 | 103.0 | 103.9 | 0.974 |
| 550 | 108.8 | 111.1 | 112.2 | 0.970 |
| 600 | 116.7 | 119.7 | 120.9 | 0.965 |
| 650 | 123.9 | 128.8 | 130.1 | 0.952 |
| 700 | 128.3 | 138.2 | 139.5 | 0.920 |
| 750 | 129.9 | 146.2 | 147.5 | 0.881 |

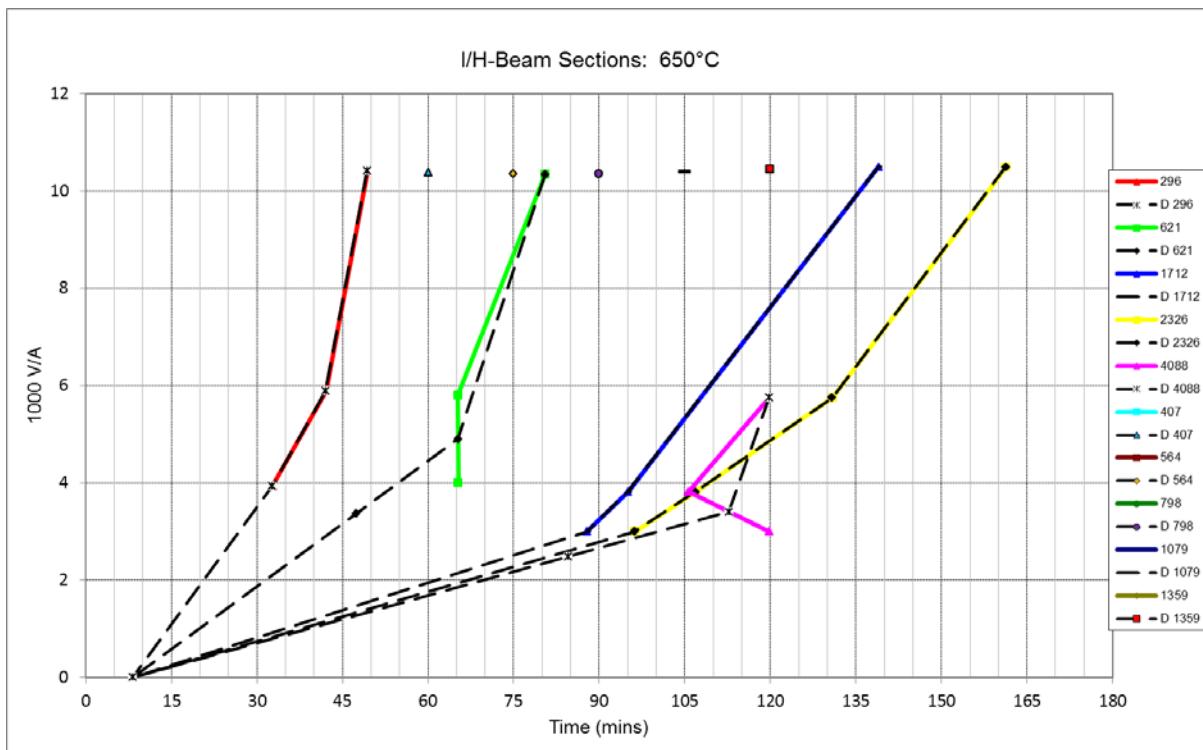
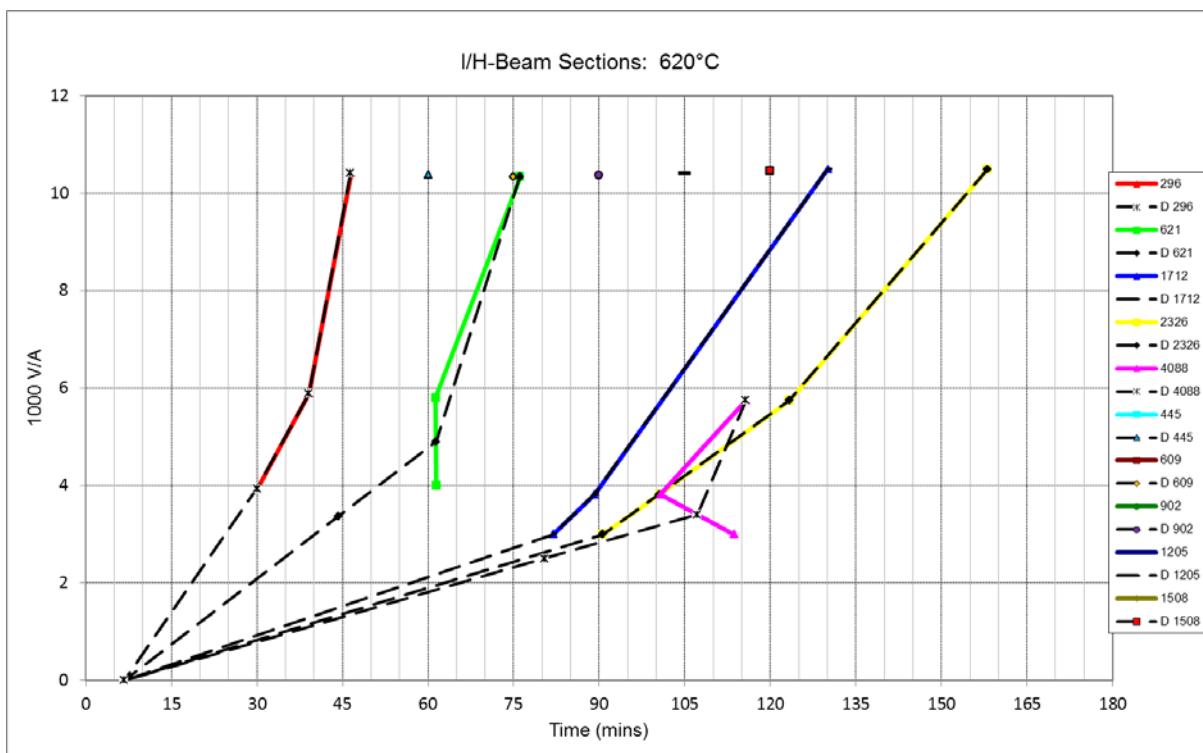
Annex A: I/H-section Beams

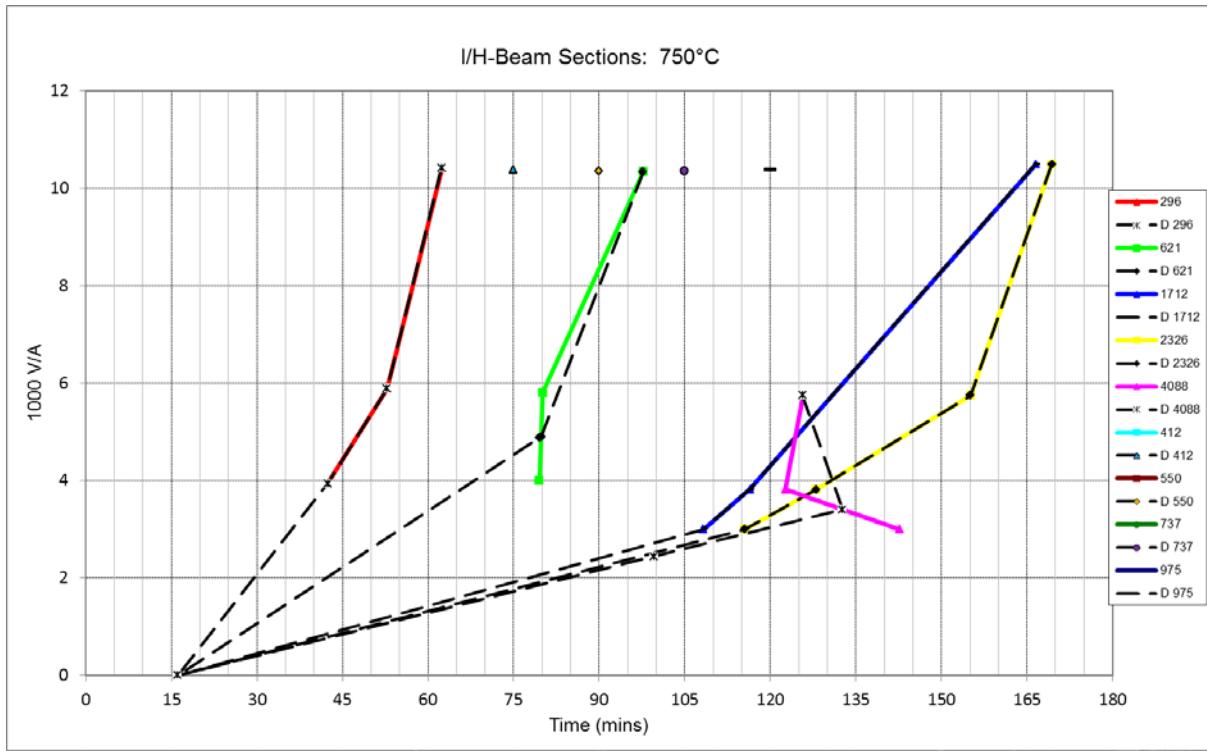
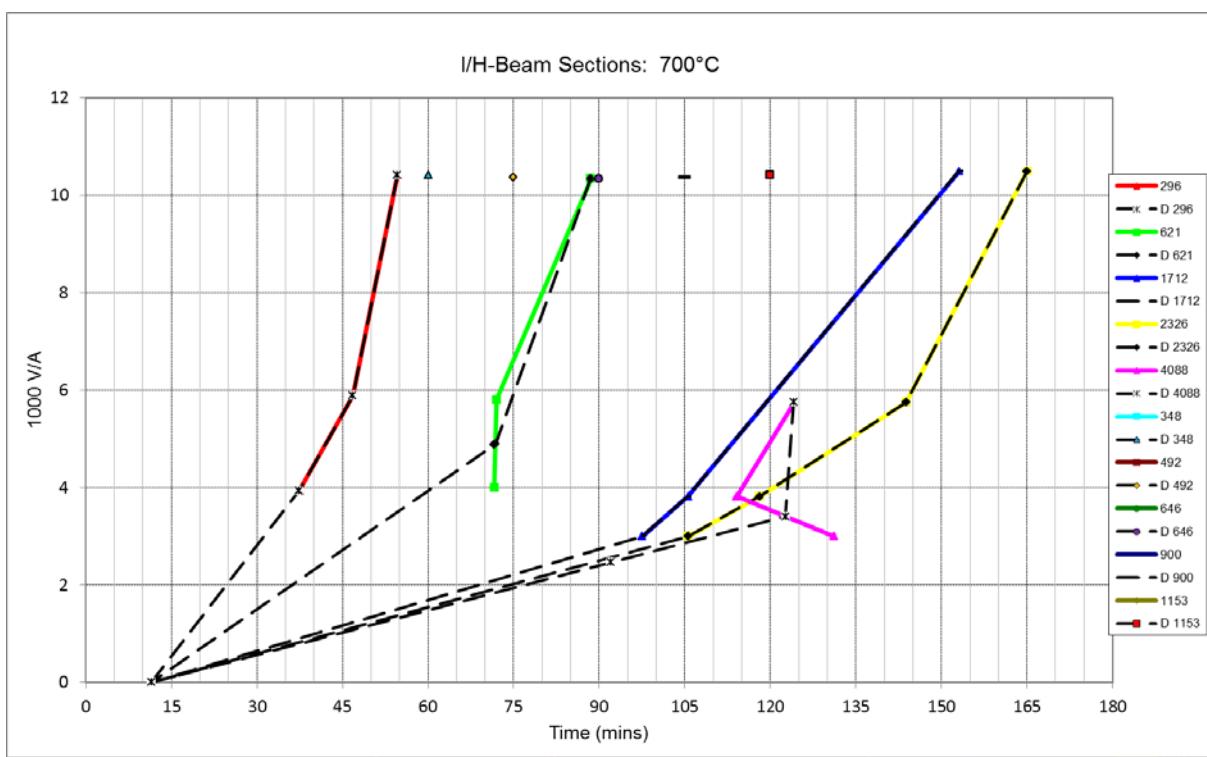
A1 Graphs: I/H-section Beams











A2 Criteria of Acceptability/Intercepts: I/H-section Beams

A2.1 Criteria of Acceptability

| Acceptability Criteria | % Allowed / Actual | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 620°C | 650°C | 700°C | 750°C |
|--------------------------------|--------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Maximum positive variation (%) | 15 | 1.71 | 2.25 | 3.37 | 4.66 | 5.53 | 6.21 | 6.43 | 6.74 | 7.49 | 8.18 |
| Optimistic predictions (%) | 30 | 12.50 | 12.50 | 12.50 | 12.50 | 12.50 | 12.50 | 12.50 | 12.50 | 6.25 | 6.25 |
| Overall conservative (%) | less than zero | -3.41 | -3.38 | -3.38 | -3.37 | -3.31 | -3.26 | -3.23 | -3.19 | -1.46 | -1.44 |

A2.2 Intercepts

| Dry Film Thickness (mm) | I/H-Beam Sections: Limiting section factor m ⁻¹ at design temperature 350°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | - | - | - | - | - | - | - |
| 0.595 | 96.7 | - | - | - | - | - | - |
| 0.621 | 103.1 | - | - | - | - | - | - |
| 1.159 | - | 96.1 | - | - | - | - | - |
| 1.712 | 407.8 | 199.4 | - | - | - | - | - |
| 1.722 | - | - | 95.3 | - | - | - | - |
| 2.113 | - | - | - | 95.3 | - | - | - |
| 2.326 | 516.1 | 340.2 | 186.1 | 116.1 | - | - | - |
| 4.088 | 653.5 | 430.7 | 321.2 | - | - | - | - |

| Dry Film Thickness (mm) | I/H-Beam Sections: Limiting section factor m ⁻¹ at design temperature 400°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | - | - | - | - | - | - | - |
| 0.384 | 96.2 | - | - | - | - | - | - |
| 0.621 | 214.1 | - | - | - | - | - | - |
| 0.787 | - | 96.6 | - | - | - | - | - |
| 1.284 | - | - | 95.9 | - | - | - | - |
| 1.712 | 507.0 | 330.9 | 150.0 | - | - | - | - |
| 1.764 | - | - | - | 95.3 | - | - | - |
| 2.137 | - | - | - | - | 95.3 | - | - |
| 2.326 | 623.8 | 409.2 | 253.0 | 170.3 | 111.9 | - | - |
| 4.088 | 753.1 | 494.0 | 367.6 | 286.8 | - | - | - |

| Dry Film Thickness (mm) | I/H-Beam Sections: Limiting section factor m ⁻¹ at design temperature 450°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 104.9 | - | - | - | - | - | - |
| 0.543 | - | 96.6 | - | - | - | - | - |
| 0.621 | 267.4 | 122.5 | - | - | - | - | - |
| 0.941 | - | - | 96.4 | - | - | - | - |
| 1.386 | - | - | - | 95.7 | - | - | - |
| 1.712 | 605.0 | 393.9 | 246.1 | 128.7 | - | - | - |
| 1.809 | - | - | - | - | 95.3 | - | - |
| 2.171 | - | - | - | - | - | 95.3 | - |
| 2.326 | 723.1 | 470.8 | 349.1 | 216.0 | 151.1 | 107.1 | - |
| 4.088 | 837.9 | 545.6 | 404.5 | 321.4 | 179.7 | - | - |

| Dry Film Thickness (mm) | I/H-Beam Sections: Limiting section factor m ⁻¹ at design temperature 500°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 139.9 | - | - | - | - | - | - |
| 0.431 | - | 96.3 | - | - | - | - | - |
| 0.621 | 320.6 | 206.4 | - | - | - | - | - |
| 0.690 | - | - | 96.7 | - | - | - | - |
| 1.088 | - | - | - | 96.2 | - | - | - |
| 1.486 | - | - | - | - | 95.6 | - | - |
| 1.712 | 711.3 | 457.9 | 337.6 | 183.0 | 115.3 | - | - |
| 1.862 | - | - | - | - | - | 95.3 | - |
| 2.208 | - | - | - | - | - | - | 95.3 |
| 2.326 | 830.9 | 534.9 | 394.4 | 277.3 | 193.8 | 138.3 | 103.5 |
| 4.088 | 929.5 | 598.3 | 441.1 | 349.4 | 266.6 | - | - |

| Dry Film Thickness (mm) | I/H-Beam Sections: Limiting section factor m ⁻¹ at design temperature 550°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 186.8 | - | - | - | - | - | - |
| 0.355 | - | 96.1 | - | - | - | - | - |
| 0.550 | - | - | 96.6 | - | - | - | - |
| 0.621 | 379.5 | 240.3 | 123.8 | - | - | - | - |
| 0.847 | - | - | - | 96.5 | - | - | - |
| 1.205 | - | - | - | - | 96.0 | - | - |
| 1.562 | - | - | - | - | - | 95.5 | - |
| 1.712 | 838.5 | 531.0 | 388.5 | 270.5 | 154.7 | 107.5 | - |
| 1.899 | - | - | - | - | - | - | 95.3 |
| 2.326 | 959.7 | 607.8 | 444.7 | 350.6 | 239.3 | 179.4 | 130.9 |
| 4.088 | 1040.4 | 658.9 | 482.1 | 380.1 | 313.7 | 175.4 | - |

| Dry Film Thickness (mm) | I/H-Beam Sections: Limiting section factor m ⁻¹ at design temperature 600°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 232.6 | - | - | - | - | - | - |
| 0.299 | - | 96.0 | - | - | - | - | - |
| 0.472 | - | - | 96.4 | - | - | - | - |
| 0.621 | 446.9 | 275.9 | 186.5 | - | - | - | - |
| 0.663 | - | - | - | 96.7 | - | - | - |
| 0.980 | - | - | - | - | 96.3 | - | - |
| 1.298 | - | - | - | - | - | 95.9 | - |
| 1.615 | - | - | - | - | - | - | 95.4 |
| 1.712 | 999.5 | 617.1 | 446.3 | 349.5 | 216.0 | 139.4 | 102.9 |
| 2.326 | 1119.6 | 691.2 | 499.9 | 391.6 | 306.6 | 218.9 | 167.9 |
| 4.088 | 1189.4 | 734.3 | 531.0 | 415.9 | 341.8 | 268.8 | - |

| Dry Film Thickness (mm) | I/H-Beam Sections: Limiting section factor m ⁻¹ at design temperature 620°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 254.0 | 104.7 | - | - | - | - | - |
| 0.445 | - | - | 96.4 | - | - | - | - |
| 0.609 | - | - | - | 96.8 | - | - | - |
| 0.621 | 479.1 | 291.5 | 209.5 | 100.8 | - | - | - |
| 0.902 | - | - | - | - | 96.4 | - | - |
| 1.205 | - | - | - | - | - | 96.0 | - |
| 1.508 | - | - | - | - | - | - | 95.6 |
| 1.712 | 1078.3 | 656.0 | 471.4 | 367.9 | 252.4 | 156.1 | 113.0 |
| 2.326 | 1203.0 | 731.9 | 525.9 | 410.4 | 336.5 | 238.3 | 182.8 |
| 4.088 | 1267.0 | 770.8 | 553.9 | 432.2 | 354.4 | 300.3 | - |

| Dry Film Thickness (mm) | I/H-Beam Sections: Limiting section factor m ⁻¹ at design temperature 650°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 285.5 | 129.1 | - | - | - | - | - |
| 0.407 | - | - | 96.3 | - | - | - | - |
| 0.564 | - | - | - | 96.7 | - | - | - |
| 0.621 | 534.3 | 316.5 | 224.9 | 119.5 | - | - | - |
| 0.798 | - | - | - | - | 96.6 | - | - |
| 1.079 | - | - | - | - | - | 96.2 | - |
| 1.359 | - | - | - | - | - | - | 95.8 |
| 1.712 | 1219.9 | 722.7 | 513.4 | 398.1 | 308.2 | 187.4 | 131.3 |
| 2.326 | 1348.7 | 798.9 | 567.6 | 440.1 | 359.4 | 272.5 | 205.1 |
| 4.088 | 1408.8 | 834.6 | 592.9 | 459.8 | 375.4 | 317.3 | - |

| Dry Film Thickness (mm) | I/H-Beam Sections: Limiting section factor m ⁻¹ at design temperature 700°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 355.7 | 181.5 | - | - | - | - | - |
| 0.348 | - | - | 96.1 | - | - | - | - |
| 0.492 | - | - | - | 96.5 | - | - | - |
| 0.621 | 665.8 | 367.7 | 254.0 | 168.7 | - | - | - |
| 0.646 | - | - | - | - | 96.8 | - | - |
| 0.900 | - | - | - | - | - | 96.4 | - |
| 1.153 | - | - | - | - | - | - | 96.1 |
| 1.712 | 1553.1 | 857.7 | 592.4 | 452.5 | 366.0 | 265.7 | 171.0 |
| 2.326 | 1699.4 | 938.5 | 648.2 | 495.1 | 400.5 | 336.2 | 252.6 |
| 4.088 | 1765.5 | 975.0 | 673.4 | 514.4 | 416.1 | 349.3 | 301.0 |

| Dry Film Thickness (mm) | I/H-Beam Sections: Limiting section factor m ⁻¹ at design temperature 750°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 480.7 | 226.1 | 107.7 | - | - | - | - |
| 0.412 | - | - | - | 96.3 | - | - | - |
| 0.550 | - | - | - | - | 96.6 | - | - |
| 0.621 | 935.9 | 450.2 | 296.3 | 220.9 | 125.2 | - | - |
| 0.737 | - | - | - | - | - | 96.6 | - |
| 0.975 | - | - | - | - | - | - | 96.3 |
| 1.712 | 2213.7 | 1064.7 | 700.9 | 522.4 | 416.4 | 346.1 | 232.8 |
| 2.326 | 2389.2 | 1149.1 | 756.5 | 563.8 | 449.4 | 373.6 | 304.3 |
| 4.088 | 2463.7 | 1185.0 | 780.1 | 581.4 | 463.4 | 385.2 | 329.6 |

Assessment limited to a maximum section factor of 368m⁻¹.

A3 Tables: I/H-section Beams

Table 1: I/H-Beam Sections 30 Minutes

| Section Factor up to m ⁻¹ | Thickness (mm) Required for a Design Temperature of | | | | | | | | | |
|--------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 620°C | 650°C | 700°C | 750°C |
| 30 | 0.567 | 0.372 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 35 | 0.567 | 0.372 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 40 | 0.567 | 0.372 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 45 | 0.567 | 0.372 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 50 | 0.567 | 0.372 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 55 | 0.567 | 0.372 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 60 | 0.567 | 0.372 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 65 | 0.567 | 0.372 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 70 | 0.567 | 0.372 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 75 | 0.567 | 0.372 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 80 | 0.567 | 0.372 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 85 | 0.567 | 0.372 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 90 | 0.567 | 0.372 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 95 | 0.588 | 0.382 | 0.276 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 100 | 0.608 | 0.392 | 0.286 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 105 | 0.628 | 0.402 | 0.296 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 110 | 0.646 | 0.412 | 0.306 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 115 | 0.664 | 0.422 | 0.316 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 120 | 0.682 | 0.432 | 0.326 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 125 | 0.699 | 0.442 | 0.336 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 130 | 0.717 | 0.452 | 0.346 | 0.278 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 135 | 0.735 | 0.462 | 0.356 | 0.287 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 140 | 0.753 | 0.472 | 0.366 | 0.296 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 145 | 0.771 | 0.482 | 0.376 | 0.305 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 150 | 0.789 | 0.492 | 0.386 | 0.314 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 155 | 0.807 | 0.502 | 0.396 | 0.323 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 160 | 0.825 | 0.512 | 0.406 | 0.332 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 165 | 0.843 | 0.522 | 0.416 | 0.341 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 170 | 0.861 | 0.532 | 0.426 | 0.350 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 175 | 0.878 | 0.542 | 0.436 | 0.359 | 0.276 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 180 | 0.896 | 0.552 | 0.446 | 0.368 | 0.284 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 185 | 0.914 | 0.563 | 0.456 | 0.377 | 0.293 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 190 | 0.932 | 0.573 | 0.466 | 0.386 | 0.301 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 195 | 0.950 | 0.583 | 0.476 | 0.395 | 0.310 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 200 | 0.968 | 0.593 | 0.486 | 0.404 | 0.318 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 205 | 0.986 | 0.603 | 0.496 | 0.413 | 0.327 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 210 | 1.004 | 0.613 | 0.506 | 0.422 | 0.335 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 215 | 1.022 | 0.624 | 0.516 | 0.431 | 0.344 | 0.275 | 0.275 | 0.275 | 0.275 | 0.275 |
| 220 | 1.040 | 0.643 | 0.526 | 0.440 | 0.352 | 0.277 | 0.275 | 0.275 | 0.275 | 0.275 |
| 225 | 1.057 | 0.662 | 0.536 | 0.449 | 0.360 | 0.284 | 0.275 | 0.275 | 0.275 | 0.275 |
| 230 | 1.075 | 0.680 | 0.546 | 0.458 | 0.369 | 0.292 | 0.275 | 0.275 | 0.275 | 0.275 |
| 235 | 1.093 | 0.699 | 0.556 | 0.467 | 0.377 | 0.300 | 0.275 | 0.275 | 0.275 | 0.275 |
| 240 | 1.111 | 0.718 | 0.566 | 0.476 | 0.386 | 0.307 | 0.276 | 0.275 | 0.275 | 0.275 |
| 245 | 1.129 | 0.736 | 0.576 | 0.485 | 0.394 | 0.315 | 0.283 | 0.275 | 0.275 | 0.275 |
| 250 | 1.147 | 0.755 | 0.586 | 0.494 | 0.403 | 0.322 | 0.290 | 0.275 | 0.275 | 0.275 |
| 255 | 1.165 | 0.773 | 0.596 | 0.503 | 0.411 | 0.330 | 0.297 | 0.275 | 0.275 | 0.275 |
| 260 | 1.183 | 0.792 | 0.606 | 0.512 | 0.419 | 0.338 | 0.305 | 0.275 | 0.275 | 0.275 |
| 265 | 1.201 | 0.811 | 0.616 | 0.521 | 0.428 | 0.345 | 0.312 | 0.275 | 0.275 | 0.275 |
| 270 | 1.219 | 0.829 | 0.629 | 0.530 | 0.436 | 0.353 | 0.319 | 0.276 | 0.275 | 0.275 |
| 275 | 1.236 | 0.848 | 0.645 | 0.539 | 0.445 | 0.360 | 0.326 | 0.282 | 0.275 | 0.275 |
| 280 | 1.254 | 0.867 | 0.662 | 0.548 | 0.453 | 0.368 | 0.333 | 0.289 | 0.275 | 0.275 |
| 285 | 1.272 | 0.885 | 0.678 | 0.557 | 0.462 | 0.375 | 0.341 | 0.295 | 0.275 | 0.275 |
| 290 | 1.290 | 0.904 | 0.694 | 0.566 | 0.470 | 0.383 | 0.348 | 0.302 | 0.275 | 0.275 |
| 295 | 1.308 | 0.922 | 0.710 | 0.575 | 0.478 | 0.391 | 0.355 | 0.308 | 0.275 | 0.275 |
| 300 | 1.326 | 0.941 | 0.726 | 0.584 | 0.487 | 0.398 | 0.362 | 0.315 | 0.275 | 0.275 |
| 305 | 1.344 | 0.960 | 0.742 | 0.593 | 0.495 | 0.406 | 0.370 | 0.321 | 0.275 | 0.275 |
| 310 | 1.362 | 0.978 | 0.759 | 0.602 | 0.504 | 0.413 | 0.377 | 0.328 | 0.275 | 0.275 |
| 315 | 1.380 | 0.997 | 0.775 | 0.611 | 0.512 | 0.421 | 0.384 | 0.335 | 0.275 | 0.275 |
| 320 | 1.398 | 1.016 | 0.791 | 0.620 | 0.521 | 0.429 | 0.391 | 0.341 | 0.275 | 0.275 |
| 325 | 1.415 | 1.034 | 0.807 | 0.633 | 0.529 | 0.436 | 0.398 | 0.348 | 0.275 | 0.275 |
| 330 | 1.433 | 1.053 | 0.823 | 0.647 | 0.538 | 0.444 | 0.406 | 0.354 | 0.275 | 0.275 |
| 335 | 1.451 | 1.071 | 0.839 | 0.661 | 0.546 | 0.451 | 0.413 | 0.361 | 0.275 | 0.275 |
| 340 | 1.469 | 1.090 | 0.856 | 0.675 | 0.554 | 0.459 | 0.420 | 0.367 | 0.280 | 0.275 |
| 345 | 1.487 | 1.109 | 0.872 | 0.689 | 0.563 | 0.466 | 0.427 | 0.374 | 0.285 | 0.275 |
| 350 | 1.505 | 1.127 | 0.888 | 0.703 | 0.571 | 0.474 | 0.435 | 0.380 | 0.290 | 0.275 |
| 355 | 1.523 | 1.146 | 0.904 | 0.717 | 0.580 | 0.482 | 0.442 | 0.387 | 0.295 | 0.275 |
| 360 | 1.541 | 1.165 | 0.920 | 0.731 | 0.588 | 0.489 | 0.449 | 0.393 | 0.301 | 0.275 |
| 365 | 1.559 | 1.183 | 0.936 | 0.745 | 0.597 | 0.497 | 0.456 | 0.400 | 0.306 | 0.275 |

Thickness is intumescent only.

Results apply to I/H-section beams with concrete slabs with 3 sided fire exposure.

| Section Factor up to m ⁻¹ | Table 2: I/H-Beam Sections 45 Minutes | | | | | | | | | |
|--------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | Thickness (mm) Required for a Design Temperature of | | | | | | | | | |
| | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 620°C | 650°C | 700°C | 750°C |
| 30 | 1.127 | 0.761 | 0.523 | 0.420 | 0.344 | 0.288 | 0.275 | 0.275 | 0.275 | 0.275 |
| 35 | 1.127 | 0.761 | 0.523 | 0.420 | 0.344 | 0.288 | 0.275 | 0.275 | 0.275 | 0.275 |
| 40 | 1.127 | 0.761 | 0.523 | 0.420 | 0.344 | 0.288 | 0.275 | 0.275 | 0.275 | 0.275 |
| 45 | 1.127 | 0.761 | 0.523 | 0.420 | 0.344 | 0.288 | 0.275 | 0.275 | 0.275 | 0.275 |
| 50 | 1.127 | 0.761 | 0.523 | 0.420 | 0.344 | 0.288 | 0.275 | 0.275 | 0.275 | 0.275 |
| 55 | 1.127 | 0.761 | 0.523 | 0.420 | 0.344 | 0.288 | 0.275 | 0.275 | 0.275 | 0.275 |
| 60 | 1.127 | 0.761 | 0.523 | 0.420 | 0.344 | 0.288 | 0.275 | 0.275 | 0.275 | 0.275 |
| 65 | 1.127 | 0.761 | 0.523 | 0.420 | 0.344 | 0.288 | 0.275 | 0.275 | 0.275 | 0.275 |
| 70 | 1.127 | 0.761 | 0.523 | 0.420 | 0.344 | 0.288 | 0.275 | 0.275 | 0.275 | 0.275 |
| 75 | 1.127 | 0.761 | 0.523 | 0.420 | 0.344 | 0.288 | 0.275 | 0.275 | 0.275 | 0.275 |
| 80 | 1.127 | 0.761 | 0.523 | 0.420 | 0.344 | 0.288 | 0.275 | 0.275 | 0.275 | 0.275 |
| 85 | 1.127 | 0.761 | 0.523 | 0.420 | 0.344 | 0.288 | 0.275 | 0.275 | 0.275 | 0.275 |
| 90 | 1.127 | 0.761 | 0.523 | 0.420 | 0.344 | 0.288 | 0.275 | 0.275 | 0.275 | 0.275 |
| 95 | 1.153 | 0.781 | 0.538 | 0.429 | 0.353 | 0.297 | 0.279 | 0.275 | 0.275 | 0.275 |
| 100 | 1.180 | 0.801 | 0.553 | 0.437 | 0.362 | 0.306 | 0.288 | 0.275 | 0.275 | 0.275 |
| 105 | 1.207 | 0.820 | 0.568 | 0.446 | 0.371 | 0.315 | 0.296 | 0.275 | 0.275 | 0.275 |
| 110 | 1.234 | 0.840 | 0.583 | 0.455 | 0.381 | 0.324 | 0.305 | 0.275 | 0.275 | 0.275 |
| 115 | 1.260 | 0.860 | 0.598 | 0.463 | 0.390 | 0.333 | 0.314 | 0.275 | 0.275 | 0.275 |
| 120 | 1.287 | 0.880 | 0.613 | 0.472 | 0.399 | 0.342 | 0.323 | 0.280 | 0.275 | 0.275 |
| 125 | 1.314 | 0.899 | 0.631 | 0.481 | 0.408 | 0.351 | 0.331 | 0.289 | 0.275 | 0.275 |
| 130 | 1.341 | 0.919 | 0.651 | 0.489 | 0.417 | 0.360 | 0.340 | 0.298 | 0.275 | 0.275 |
| 135 | 1.367 | 0.939 | 0.671 | 0.498 | 0.427 | 0.369 | 0.349 | 0.306 | 0.275 | 0.275 |
| 140 | 1.394 | 0.958 | 0.691 | 0.506 | 0.436 | 0.378 | 0.357 | 0.315 | 0.275 | 0.275 |
| 145 | 1.421 | 0.978 | 0.711 | 0.515 | 0.445 | 0.387 | 0.366 | 0.324 | 0.275 | 0.275 |
| 150 | 1.448 | 0.998 | 0.731 | 0.524 | 0.454 | 0.396 | 0.375 | 0.332 | 0.275 | 0.275 |
| 155 | 1.475 | 1.018 | 0.751 | 0.532 | 0.464 | 0.405 | 0.383 | 0.341 | 0.275 | 0.275 |
| 160 | 1.501 | 1.037 | 0.772 | 0.541 | 0.473 | 0.414 | 0.392 | 0.350 | 0.275 | 0.275 |
| 165 | 1.528 | 1.057 | 0.792 | 0.550 | 0.482 | 0.423 | 0.401 | 0.358 | 0.275 | 0.275 |
| 170 | 1.555 | 1.077 | 0.812 | 0.558 | 0.491 | 0.431 | 0.410 | 0.367 | 0.276 | 0.275 |
| 175 | 1.582 | 1.097 | 0.832 | 0.567 | 0.501 | 0.440 | 0.418 | 0.376 | 0.285 | 0.275 |
| 180 | 1.608 | 1.116 | 0.852 | 0.575 | 0.510 | 0.449 | 0.427 | 0.384 | 0.293 | 0.275 |
| 185 | 1.635 | 1.136 | 0.872 | 0.584 | 0.519 | 0.458 | 0.436 | 0.393 | 0.302 | 0.275 |
| 190 | 1.662 | 1.156 | 0.892 | 0.593 | 0.528 | 0.467 | 0.444 | 0.402 | 0.311 | 0.275 |
| 195 | 1.689 | 1.176 | 0.912 | 0.601 | 0.537 | 0.476 | 0.453 | 0.410 | 0.320 | 0.275 |
| 200 | 1.715 | 1.195 | 0.932 | 0.610 | 0.547 | 0.485 | 0.462 | 0.419 | 0.328 | 0.275 |
| 205 | 1.737 | 1.215 | 0.952 | 0.619 | 0.556 | 0.494 | 0.470 | 0.428 | 0.337 | 0.275 |
| 210 | 1.758 | 1.235 | 0.973 | 0.637 | 0.565 | 0.503 | 0.479 | 0.436 | 0.346 | 0.275 |
| 215 | 1.780 | 1.255 | 0.993 | 0.658 | 0.574 | 0.512 | 0.488 | 0.445 | 0.355 | 0.280 |
| 220 | 1.802 | 1.274 | 1.013 | 0.680 | 0.584 | 0.521 | 0.497 | 0.454 | 0.363 | 0.287 |
| 225 | 1.824 | 1.294 | 1.033 | 0.702 | 0.593 | 0.530 | 0.505 | 0.462 | 0.372 | 0.294 |
| 230 | 1.846 | 1.314 | 1.053 | 0.723 | 0.602 | 0.539 | 0.514 | 0.471 | 0.381 | 0.302 |
| 235 | 1.867 | 1.334 | 1.073 | 0.745 | 0.611 | 0.548 | 0.523 | 0.480 | 0.389 | 0.309 |
| 240 | 1.889 | 1.353 | 1.093 | 0.767 | 0.620 | 0.557 | 0.531 | 0.488 | 0.398 | 0.316 |
| 245 | 1.911 | 1.373 | 1.113 | 0.788 | 0.639 | 0.566 | 0.540 | 0.497 | 0.407 | 0.323 |
| 250 | 1.933 | 1.393 | 1.133 | 0.810 | 0.657 | 0.575 | 0.549 | 0.506 | 0.416 | 0.331 |
| 255 | 1.955 | 1.413 | 1.153 | 0.832 | 0.676 | 0.584 | 0.558 | 0.514 | 0.424 | 0.338 |
| 260 | 1.976 | 1.432 | 1.174 | 0.854 | 0.695 | 0.593 | 0.566 | 0.523 | 0.433 | 0.345 |
| 265 | 1.998 | 1.452 | 1.194 | 0.875 | 0.714 | 0.602 | 0.575 | 0.532 | 0.442 | 0.352 |
| 270 | 2.020 | 1.472 | 1.214 | 0.897 | 0.732 | 0.610 | 0.584 | 0.540 | 0.451 | 0.360 |
| 275 | 2.042 | 1.491 | 1.234 | 0.919 | 0.751 | 0.619 | 0.592 | 0.549 | 0.459 | 0.367 |
| 280 | 2.064 | 1.511 | 1.254 | 0.940 | 0.770 | 0.634 | 0.601 | 0.558 | 0.468 | 0.374 |
| 285 | 2.085 | 1.531 | 1.274 | 0.962 | 0.789 | 0.650 | 0.610 | 0.566 | 0.477 | 0.381 |
| 290 | 2.107 | 1.551 | 1.294 | 0.984 | 0.807 | 0.666 | 0.618 | 0.575 | 0.485 | 0.389 |
| 295 | 2.129 | 1.570 | 1.314 | 1.005 | 0.826 | 0.682 | 0.632 | 0.584 | 0.494 | 0.396 |
| 300 | 2.151 | 1.590 | 1.334 | 1.027 | 0.845 | 0.698 | 0.646 | 0.592 | 0.503 | 0.403 |
| 305 | 2.173 | 1.610 | 1.355 | 1.049 | 0.864 | 0.714 | 0.661 | 0.601 | 0.512 | 0.410 |
| 310 | 2.194 | 1.630 | 1.375 | 1.070 | 0.883 | 0.730 | 0.676 | 0.610 | 0.520 | 0.418 |
| 315 | 2.216 | 1.649 | 1.395 | 1.092 | 0.901 | 0.746 | 0.691 | 0.618 | 0.529 | 0.425 |
| 320 | 2.238 | 1.669 | 1.415 | 1.114 | 0.920 | 0.762 | 0.706 | 0.630 | 0.538 | 0.432 |
| 325 | 2.260 | 1.689 | 1.435 | 1.135 | 0.939 | 0.778 | 0.721 | 0.644 | 0.547 | 0.439 |
| 330 | 2.282 | 1.709 | 1.455 | 1.157 | 0.958 | 0.794 | 0.736 | 0.657 | 0.555 | 0.447 |
| 335 | 2.303 | 1.744 | 1.475 | 1.179 | 0.976 | 0.810 | 0.751 | 0.671 | 0.564 | 0.454 |
| 340 | 2.325 | 1.784 | 1.495 | 1.201 | 0.995 | 0.826 | 0.766 | 0.684 | 0.573 | 0.461 |
| 345 | 2.420 | 1.823 | 1.515 | 1.222 | 1.014 | 0.842 | 0.781 | 0.698 | 0.581 | 0.468 |
| 350 | 2.517 | 1.862 | 1.535 | 1.244 | 1.033 | 0.858 | 0.796 | 0.711 | 0.590 | 0.476 |
| 355 | 2.615 | 1.901 | 1.556 | 1.266 | 1.051 | 0.874 | 0.811 | 0.724 | 0.599 | 0.483 |
| 360 | 2.712 | 1.940 | 1.576 | 1.287 | 1.070 | 0.890 | 0.826 | 0.738 | 0.608 | 0.490 |
| 365 | 2.809 | 1.980 | 1.596 | 1.309 | 1.089 | 0.906 | 0.841 | 0.751 | 0.616 | 0.497 |

Thickness is intumescent only.

Results apply to I/H-section beams with concrete slabs with 3 sided fire exposure.

| Section Factor up to m ⁻¹ | Thickness (mm) Required for a Design Temperature of | | | | | | | | | |
|--------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 620°C | 650°C | 700°C | 750°C |
| 30 | 1.687 | 1.238 | 0.908 | 0.662 | 0.533 | 0.461 | 0.435 | 0.397 | 0.337 | 0.275 |
| 35 | 1.687 | 1.238 | 0.908 | 0.662 | 0.533 | 0.461 | 0.435 | 0.397 | 0.337 | 0.275 |
| 40 | 1.687 | 1.238 | 0.908 | 0.662 | 0.533 | 0.461 | 0.435 | 0.397 | 0.337 | 0.275 |
| 45 | 1.687 | 1.238 | 0.908 | 0.662 | 0.533 | 0.461 | 0.435 | 0.397 | 0.337 | 0.275 |
| 50 | 1.687 | 1.238 | 0.908 | 0.662 | 0.533 | 0.461 | 0.435 | 0.397 | 0.337 | 0.275 |
| 55 | 1.687 | 1.238 | 0.908 | 0.662 | 0.533 | 0.461 | 0.435 | 0.397 | 0.337 | 0.275 |
| 60 | 1.687 | 1.238 | 0.908 | 0.662 | 0.533 | 0.461 | 0.435 | 0.397 | 0.337 | 0.275 |
| 65 | 1.687 | 1.238 | 0.908 | 0.662 | 0.533 | 0.461 | 0.435 | 0.397 | 0.337 | 0.275 |
| 70 | 1.687 | 1.238 | 0.908 | 0.662 | 0.533 | 0.461 | 0.435 | 0.397 | 0.337 | 0.275 |
| 75 | 1.687 | 1.238 | 0.908 | 0.662 | 0.533 | 0.461 | 0.435 | 0.397 | 0.337 | 0.275 |
| 80 | 1.687 | 1.238 | 0.908 | 0.662 | 0.533 | 0.461 | 0.435 | 0.397 | 0.337 | 0.275 |
| 85 | 1.687 | 1.238 | 0.908 | 0.662 | 0.533 | 0.461 | 0.435 | 0.397 | 0.337 | 0.275 |
| 90 | 1.687 | 1.238 | 0.908 | 0.662 | 0.533 | 0.461 | 0.435 | 0.397 | 0.337 | 0.275 |
| 95 | 1.720 | 1.277 | 0.934 | 0.683 | 0.546 | 0.470 | 0.443 | 0.405 | 0.346 | 0.275 |
| 100 | 1.753 | 1.317 | 0.960 | 0.704 | 0.559 | 0.478 | 0.451 | 0.413 | 0.355 | 0.283 |
| 105 | 1.787 | 1.356 | 0.985 | 0.725 | 0.572 | 0.486 | 0.458 | 0.422 | 0.363 | 0.291 |
| 110 | 1.820 | 1.396 | 1.011 | 0.746 | 0.585 | 0.494 | 0.466 | 0.430 | 0.372 | 0.300 |
| 115 | 1.853 | 1.435 | 1.037 | 0.768 | 0.598 | 0.503 | 0.474 | 0.438 | 0.381 | 0.309 |
| 120 | 1.886 | 1.475 | 1.063 | 0.789 | 0.611 | 0.511 | 0.482 | 0.447 | 0.389 | 0.317 |
| 125 | 1.919 | 1.514 | 1.088 | 0.810 | 0.626 | 0.519 | 0.490 | 0.455 | 0.398 | 0.326 |
| 130 | 1.953 | 1.554 | 1.114 | 0.831 | 0.646 | 0.528 | 0.497 | 0.463 | 0.407 | 0.334 |
| 135 | 1.986 | 1.593 | 1.140 | 0.852 | 0.667 | 0.536 | 0.505 | 0.471 | 0.415 | 0.343 |
| 140 | 2.019 | 1.633 | 1.166 | 0.874 | 0.688 | 0.544 | 0.513 | 0.480 | 0.424 | 0.352 |
| 145 | 2.052 | 1.672 | 1.191 | 0.895 | 0.708 | 0.552 | 0.521 | 0.488 | 0.433 | 0.360 |
| 150 | 2.086 | 1.712 | 1.217 | 0.916 | 0.729 | 0.561 | 0.528 | 0.496 | 0.441 | 0.369 |
| 155 | 2.119 | 1.742 | 1.243 | 0.937 | 0.749 | 0.569 | 0.536 | 0.505 | 0.450 | 0.377 |
| 160 | 2.152 | 1.771 | 1.269 | 0.959 | 0.770 | 0.577 | 0.544 | 0.513 | 0.458 | 0.386 |
| 165 | 2.185 | 1.801 | 1.294 | 0.980 | 0.791 | 0.585 | 0.552 | 0.521 | 0.467 | 0.395 |
| 170 | 2.219 | 1.831 | 1.320 | 1.001 | 0.811 | 0.594 | 0.560 | 0.530 | 0.476 | 0.403 |
| 175 | 2.252 | 1.861 | 1.346 | 1.022 | 0.832 | 0.602 | 0.567 | 0.538 | 0.484 | 0.412 |
| 180 | 2.285 | 1.891 | 1.372 | 1.043 | 0.853 | 0.610 | 0.575 | 0.546 | 0.493 | 0.421 |
| 185 | 2.318 | 1.920 | 1.397 | 1.065 | 0.873 | 0.619 | 0.583 | 0.555 | 0.502 | 0.429 |
| 190 | 2.376 | 1.950 | 1.423 | 1.086 | 0.894 | 0.636 | 0.591 | 0.563 | 0.510 | 0.438 |
| 195 | 2.442 | 1.980 | 1.449 | 1.107 | 0.914 | 0.657 | 0.599 | 0.571 | 0.519 | 0.446 |
| 200 | 2.507 | 2.010 | 1.474 | 1.128 | 0.935 | 0.678 | 0.606 | 0.580 | 0.528 | 0.455 |
| 205 | 2.572 | 2.040 | 1.500 | 1.149 | 0.956 | 0.699 | 0.614 | 0.588 | 0.536 | 0.464 |
| 210 | 2.637 | 2.070 | 1.526 | 1.171 | 0.976 | 0.720 | 0.623 | 0.596 | 0.545 | 0.472 |
| 215 | 2.703 | 2.099 | 1.552 | 1.192 | 0.997 | 0.741 | 0.644 | 0.605 | 0.554 | 0.481 |
| 220 | 2.768 | 2.129 | 1.577 | 1.213 | 1.017 | 0.762 | 0.665 | 0.613 | 0.562 | 0.489 |
| 225 | 2.833 | 2.159 | 1.603 | 1.234 | 1.038 | 0.783 | 0.686 | 0.622 | 0.571 | 0.498 |
| 230 | 2.898 | 2.189 | 1.629 | 1.255 | 1.059 | 0.804 | 0.707 | 0.640 | 0.580 | 0.507 |
| 235 | 2.963 | 2.219 | 1.655 | 1.277 | 1.079 | 0.825 | 0.727 | 0.659 | 0.588 | 0.515 |
| 240 | 3.029 | 2.249 | 1.680 | 1.298 | 1.100 | 0.846 | 0.748 | 0.678 | 0.597 | 0.524 |
| 245 | 3.094 | 2.278 | 1.706 | 1.319 | 1.120 | 0.867 | 0.769 | 0.697 | 0.605 | 0.533 |
| 250 | 3.159 | 2.308 | 1.735 | 1.340 | 1.141 | 0.888 | 0.790 | 0.716 | 0.614 | 0.541 |
| 255 | 3.224 | 2.357 | 1.765 | 1.362 | 1.162 | 0.909 | 0.811 | 0.735 | 0.624 | 0.550 |
| 260 | 3.290 | 2.434 | 1.795 | 1.383 | 1.182 | 0.930 | 0.832 | 0.754 | 0.640 | 0.558 |
| 265 | 3.355 | 2.511 | 1.824 | 1.404 | 1.203 | 0.951 | 0.852 | 0.773 | 0.657 | 0.567 |
| 270 | 3.420 | 2.588 | 1.854 | 1.425 | 1.224 | 0.972 | 0.873 | 0.792 | 0.673 | 0.576 |
| 275 | 3.485 | 2.664 | 1.884 | 1.446 | 1.244 | 0.993 | 0.894 | 0.811 | 0.689 | 0.584 |
| 280 | 3.551 | 2.741 | 1.914 | 1.468 | 1.265 | 1.014 | 0.915 | 0.829 | 0.705 | 0.593 |
| 285 | 3.616 | 2.818 | 1.944 | 1.489 | 1.285 | 1.035 | 0.936 | 0.848 | 0.721 | 0.601 |
| 290 | 3.681 | 2.895 | 1.974 | 1.510 | 1.306 | 1.056 | 0.956 | 0.867 | 0.737 | 0.610 |
| 295 | 3.746 | 2.972 | 2.003 | 1.531 | 1.327 | 1.077 | 0.977 | 0.886 | 0.753 | 0.619 |
| 300 | 3.811 | 3.049 | 2.033 | 1.552 | 1.347 | 1.098 | 0.998 | 0.905 | 0.769 | 0.631 |
| 305 | 3.877 | 3.126 | 2.063 | 1.574 | 1.368 | 1.119 | 1.019 | 0.924 | 0.786 | 0.644 |
| 310 | - | 3.203 | 2.093 | 1.595 | 1.388 | 1.140 | 1.040 | 0.943 | 0.802 | 0.658 |
| 315 | - | 3.280 | 2.123 | 1.616 | 1.409 | 1.161 | 1.061 | 0.962 | 0.818 | 0.671 |
| 320 | - | 3.356 | 2.153 | 1.637 | 1.430 | 1.182 | 1.081 | 0.981 | 0.834 | 0.685 |
| 325 | - | 3.433 | 2.182 | 1.659 | 1.450 | 1.203 | 1.102 | 1.000 | 0.850 | 0.698 |
| 330 | - | 3.510 | 2.212 | 1.680 | 1.471 | 1.224 | 1.123 | 1.019 | 0.866 | 0.712 |
| 335 | - | 3.587 | 2.242 | 1.701 | 1.491 | 1.245 | 1.144 | 1.037 | 0.882 | 0.725 |
| 340 | - | 3.664 | 2.272 | 1.738 | 1.512 | 1.266 | 1.165 | 1.056 | 0.898 | 0.739 |
| 345 | - | 3.741 | 2.302 | 1.792 | 1.533 | 1.287 | 1.186 | 1.075 | 0.914 | 0.752 |
| 350 | - | 3.818 | 2.355 | 1.846 | 1.553 | 1.308 | 1.206 | 1.094 | 0.931 | 0.766 |
| 355 | - | 3.895 | 2.514 | 1.900 | 1.574 | 1.329 | 1.227 | 1.113 | 0.947 | 0.779 |
| 360 | - | - | 2.673 | 1.954 | 1.595 | 1.350 | 1.248 | 1.132 | 0.963 | 0.793 |
| 365 | - | - | 2.832 | 2.008 | 1.615 | 1.371 | 1.269 | 1.151 | 0.979 | 0.806 |

Thickness is intumescent only.

Results apply to I/H-section beams with concrete slabs with 3 sided fire exposure.

| Section Factor up to m ⁻¹ | Table 4: I/H-Beam Sections 75 Minutes | | | | | | | | | |
|--------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | Thickness (mm) Required for a Design Temperature of | | | | | | | | | |
| | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 620°C | 650°C | 700°C | 750°C |
| 30 | 2.059 | 1.724 | 1.329 | 1.044 | 0.815 | 0.635 | 0.589 | 0.547 | 0.480 | 0.401 |
| 35 | 2.059 | 1.724 | 1.329 | 1.044 | 0.815 | 0.635 | 0.589 | 0.547 | 0.480 | 0.401 |
| 40 | 2.059 | 1.724 | 1.329 | 1.044 | 0.815 | 0.635 | 0.589 | 0.547 | 0.480 | 0.401 |
| 45 | 2.059 | 1.724 | 1.329 | 1.044 | 0.815 | 0.635 | 0.589 | 0.547 | 0.480 | 0.401 |
| 50 | 2.059 | 1.724 | 1.329 | 1.044 | 0.815 | 0.635 | 0.589 | 0.547 | 0.480 | 0.401 |
| 55 | 2.059 | 1.724 | 1.329 | 1.044 | 0.815 | 0.635 | 0.589 | 0.547 | 0.480 | 0.401 |
| 60 | 2.059 | 1.724 | 1.329 | 1.044 | 0.815 | 0.635 | 0.589 | 0.547 | 0.480 | 0.401 |
| 65 | 2.059 | 1.724 | 1.329 | 1.044 | 0.815 | 0.635 | 0.589 | 0.547 | 0.480 | 0.401 |
| 70 | 2.059 | 1.724 | 1.329 | 1.044 | 0.815 | 0.635 | 0.589 | 0.547 | 0.480 | 0.401 |
| 75 | 2.059 | 1.724 | 1.329 | 1.044 | 0.815 | 0.635 | 0.589 | 0.547 | 0.480 | 0.401 |
| 80 | 2.059 | 1.724 | 1.329 | 1.044 | 0.815 | 0.635 | 0.589 | 0.547 | 0.480 | 0.401 |
| 85 | 2.059 | 1.724 | 1.329 | 1.044 | 0.815 | 0.635 | 0.589 | 0.547 | 0.480 | 0.401 |
| 90 | 2.059 | 1.724 | 1.329 | 1.044 | 0.815 | 0.635 | 0.589 | 0.547 | 0.480 | 0.401 |
| 95 | 2.110 | 1.762 | 1.379 | 1.080 | 0.840 | 0.656 | 0.604 | 0.560 | 0.489 | 0.410 |
| 100 | 2.161 | 1.799 | 1.428 | 1.116 | 0.864 | 0.677 | 0.609 | 0.572 | 0.498 | 0.418 |
| 105 | 2.212 | 1.837 | 1.478 | 1.152 | 0.889 | 0.697 | 0.638 | 0.585 | 0.507 | 0.427 |
| 110 | 2.264 | 1.874 | 1.527 | 1.187 | 0.914 | 0.718 | 0.659 | 0.597 | 0.516 | 0.435 |
| 115 | 2.315 | 1.912 | 1.577 | 1.223 | 0.939 | 0.739 | 0.679 | 0.610 | 0.525 | 0.443 |
| 120 | 2.366 | 1.949 | 1.626 | 1.259 | 0.964 | 0.760 | 0.700 | 0.623 | 0.534 | 0.452 |
| 125 | 2.417 | 1.987 | 1.676 | 1.295 | 0.989 | 0.780 | 0.720 | 0.643 | 0.543 | 0.460 |
| 130 | 2.469 | 2.024 | 1.721 | 1.331 | 1.014 | 0.801 | 0.740 | 0.662 | 0.552 | 0.469 |
| 135 | 2.520 | 2.062 | 1.757 | 1.367 | 1.038 | 0.822 | 0.761 | 0.682 | 0.561 | 0.477 |
| 140 | 2.571 | 2.099 | 1.792 | 1.403 | 1.063 | 0.842 | 0.781 | 0.701 | 0.570 | 0.485 |
| 145 | 2.622 | 2.137 | 1.827 | 1.439 | 1.088 | 0.863 | 0.802 | 0.721 | 0.579 | 0.494 |
| 150 | 2.674 | 2.174 | 1.862 | 1.475 | 1.113 | 0.884 | 0.822 | 0.740 | 0.588 | 0.502 |
| 155 | 2.725 | 2.212 | 1.897 | 1.511 | 1.138 | 0.905 | 0.843 | 0.760 | 0.597 | 0.511 |
| 160 | 2.776 | 2.249 | 1.932 | 1.547 | 1.163 | 0.925 | 0.863 | 0.780 | 0.605 | 0.519 |
| 165 | 2.827 | 2.287 | 1.967 | 1.582 | 1.187 | 0.946 | 0.883 | 0.799 | 0.614 | 0.527 |
| 170 | 2.879 | 2.324 | 2.003 | 1.618 | 1.212 | 0.967 | 0.904 | 0.819 | 0.626 | 0.536 |
| 175 | 2.930 | 2.398 | 2.038 | 1.654 | 1.237 | 0.988 | 0.924 | 0.838 | 0.645 | 0.544 |
| 180 | 2.981 | 2.473 | 2.073 | 1.690 | 1.262 | 1.008 | 0.945 | 0.858 | 0.664 | 0.552 |
| 185 | 3.032 | 2.549 | 2.108 | 1.725 | 1.287 | 1.029 | 0.965 | 0.878 | 0.684 | 0.561 |
| 190 | 3.083 | 2.624 | 2.143 | 1.757 | 1.312 | 1.050 | 0.986 | 0.897 | 0.703 | 0.569 |
| 195 | 3.135 | 2.700 | 2.178 | 1.790 | 1.337 | 1.071 | 1.006 | 0.917 | 0.722 | 0.578 |
| 200 | 3.186 | 2.776 | 2.213 | 1.823 | 1.361 | 1.091 | 1.026 | 0.936 | 0.741 | 0.586 |
| 205 | 3.237 | 2.851 | 2.248 | 1.855 | 1.386 | 1.112 | 1.047 | 0.956 | 0.761 | 0.594 |
| 210 | 3.288 | 2.927 | 2.284 | 1.888 | 1.411 | 1.133 | 1.067 | 0.975 | 0.780 | 0.603 |
| 215 | 3.340 | 3.002 | 2.319 | 1.920 | 1.436 | 1.154 | 1.088 | 0.995 | 0.799 | 0.611 |
| 220 | 3.391 | 3.078 | 2.392 | 1.953 | 1.461 | 1.174 | 1.108 | 1.015 | 0.818 | 0.620 |
| 225 | 3.442 | 3.154 | 2.476 | 1.985 | 1.486 | 1.195 | 1.128 | 1.034 | 0.837 | 0.636 |
| 230 | 3.493 | 3.229 | 2.560 | 2.018 | 1.510 | 1.216 | 1.149 | 1.054 | 0.857 | 0.654 |
| 235 | 3.545 | 3.305 | 2.643 | 2.051 | 1.535 | 1.237 | 1.169 | 1.073 | 0.876 | 0.672 |
| 240 | 3.596 | 3.380 | 2.727 | 2.083 | 1.560 | 1.257 | 1.190 | 1.093 | 0.895 | 0.690 |
| 245 | 3.647 | 3.456 | 2.811 | 2.116 | 1.585 | 1.278 | 1.210 | 1.112 | 0.914 | 0.708 |
| 250 | 3.698 | 3.532 | 2.894 | 2.148 | 1.610 | 1.299 | 1.231 | 1.132 | 0.934 | 0.726 |
| 255 | 3.750 | 3.607 | 2.978 | 2.181 | 1.635 | 1.320 | 1.251 | 1.152 | 0.953 | 0.744 |
| 260 | 3.801 | 3.683 | 3.061 | 2.213 | 1.660 | 1.340 | 1.271 | 1.171 | 0.972 | 0.763 |
| 265 | 3.852 | 3.759 | 3.145 | 2.246 | 1.684 | 1.361 | 1.292 | 1.191 | 0.991 | 0.781 |
| 270 | 3.903 | 3.834 | 3.229 | 2.279 | 1.709 | 1.382 | 1.312 | 1.210 | 1.010 | 0.799 |
| 275 | - | - | 3.312 | 2.311 | 1.746 | 1.403 | 1.333 | 1.230 | 1.030 | 0.817 |
| 280 | - | - | 3.396 | 2.393 | 1.784 | 1.423 | 1.353 | 1.250 | 1.049 | 0.835 |
| 285 | - | - | 3.480 | 2.515 | 1.823 | 1.444 | 1.374 | 1.269 | 1.068 | 0.853 |
| 290 | - | - | 3.563 | 2.637 | 1.861 | 1.465 | 1.394 | 1.289 | 1.087 | 0.871 |
| 295 | - | - | 3.647 | 2.759 | 1.900 | 1.486 | 1.414 | 1.308 | 1.107 | 0.889 |
| 300 | - | - | 3.731 | 2.882 | 1.938 | 1.506 | 1.435 | 1.328 | 1.126 | 0.907 |
| 305 | - | - | 3.814 | 3.004 | 1.976 | 1.527 | 1.455 | 1.347 | 1.145 | 0.925 |
| 310 | - | - | 3.898 | 3.126 | 2.015 | 1.548 | 1.476 | 1.367 | 1.164 | 0.943 |
| 315 | - | - | - | 3.248 | 2.053 | 1.569 | 1.496 | 1.387 | 1.183 | 0.962 |
| 320 | - | - | - | 3.370 | 2.091 | 1.589 | 1.517 | 1.406 | 1.203 | 0.980 |
| 325 | - | - | - | 3.493 | 2.130 | 1.610 | 1.537 | 1.426 | 1.222 | 0.998 |
| 330 | - | - | - | 3.615 | 2.168 | 1.631 | 1.557 | 1.445 | 1.241 | 1.016 |
| 335 | - | - | - | 3.737 | 2.206 | 1.652 | 1.578 | 1.465 | 1.260 | 1.034 |
| 340 | - | - | - | 3.859 | 2.245 | 1.672 | 1.598 | 1.484 | 1.280 | 1.052 |
| 345 | - | - | - | - | 2.283 | 1.693 | 1.619 | 1.504 | 1.299 | 1.070 |
| 350 | - | - | - | - | 2.321 | 1.719 | 1.639 | 1.524 | 1.318 | 1.088 |
| 355 | - | - | - | - | 2.589 | 1.792 | 1.660 | 1.543 | 1.337 | 1.106 |
| 360 | - | - | - | - | 2.888 | 1.865 | 1.680 | 1.563 | 1.356 | 1.124 |
| 365 | - | - | - | - | 3.187 | 1.938 | 1.700 | 1.582 | 1.376 | 1.142 |

Thickness is intumescent only.

Results apply to I/H-section beams with concrete slabs with 3 sided fire exposure.

Table 5: I/H-Beam Sections 90 Minutes

| Section Factor up to m ⁻¹ | Thickness (mm) Required for a Design Temperature of | | | | | | | | | |
|--------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 620°C | 650°C | 700°C | 750°C |
| 30 | - | 2.077 | 1.760 | 1.422 | 1.153 | 0.941 | 0.869 | 0.770 | 0.619 | 0.534 |
| 35 | - | 2.077 | 1.760 | 1.422 | 1.153 | 0.941 | 0.869 | 0.770 | 0.619 | 0.534 |
| 40 | - | 2.077 | 1.760 | 1.422 | 1.153 | 0.941 | 0.869 | 0.770 | 0.619 | 0.534 |
| 45 | - | 2.077 | 1.760 | 1.422 | 1.153 | 0.941 | 0.869 | 0.770 | 0.619 | 0.534 |
| 50 | - | 2.077 | 1.760 | 1.422 | 1.153 | 0.941 | 0.869 | 0.770 | 0.619 | 0.534 |
| 55 | - | 2.077 | 1.760 | 1.422 | 1.153 | 0.941 | 0.869 | 0.770 | 0.619 | 0.534 |
| 60 | - | 2.077 | 1.760 | 1.422 | 1.153 | 0.941 | 0.869 | 0.770 | 0.619 | 0.534 |
| 65 | - | 2.077 | 1.760 | 1.422 | 1.153 | 0.941 | 0.869 | 0.770 | 0.619 | 0.534 |
| 70 | - | 2.077 | 1.760 | 1.422 | 1.153 | 0.941 | 0.869 | 0.770 | 0.619 | 0.534 |
| 75 | - | 2.077 | 1.760 | 1.422 | 1.153 | 0.941 | 0.869 | 0.770 | 0.619 | 0.534 |
| 80 | - | 2.077 | 1.760 | 1.422 | 1.153 | 0.941 | 0.869 | 0.770 | 0.619 | 0.534 |
| 85 | - | 2.077 | 1.760 | 1.422 | 1.153 | 0.941 | 0.869 | 0.770 | 0.619 | 0.534 |
| 90 | - | 2.077 | 1.760 | 1.422 | 1.153 | 0.941 | 0.869 | 0.770 | 0.619 | 0.534 |
| 95 | - | 2.134 | 1.806 | 1.479 | 1.196 | 0.972 | 0.895 | 0.791 | 0.639 | 0.546 |
| 100 | - | 2.191 | 1.853 | 1.536 | 1.240 | 1.003 | 0.921 | 0.813 | 0.659 | 0.558 |
| 105 | - | 2.248 | 1.899 | 1.594 | 1.283 | 1.033 | 0.947 | 0.834 | 0.679 | 0.571 |
| 110 | - | 2.305 | 1.945 | 1.651 | 1.326 | 1.064 | 0.973 | 0.856 | 0.698 | 0.583 |
| 115 | - | 2.362 | 1.992 | 1.709 | 1.369 | 1.094 | 0.999 | 0.878 | 0.718 | 0.596 |
| 120 | - | 2.419 | 2.038 | 1.749 | 1.412 | 1.125 | 1.024 | 0.899 | 0.738 | 0.608 |
| 125 | - | 2.476 | 2.084 | 1.788 | 1.455 | 1.155 | 1.050 | 0.921 | 0.758 | 0.621 |
| 130 | - | 2.533 | 2.131 | 1.827 | 1.499 | 1.186 | 1.076 | 0.942 | 0.778 | 0.639 |
| 135 | - | 2.590 | 2.177 | 1.866 | 1.542 | 1.217 | 1.102 | 0.964 | 0.797 | 0.658 |
| 140 | - | 2.647 | 2.223 | 1.905 | 1.585 | 1.247 | 1.128 | 0.986 | 0.817 | 0.677 |
| 145 | - | 2.704 | 2.270 | 1.944 | 1.628 | 1.278 | 1.154 | 1.007 | 0.837 | 0.695 |
| 150 | - | 2.761 | 2.316 | 1.983 | 1.671 | 1.308 | 1.180 | 1.029 | 0.857 | 0.714 |
| 155 | - | 2.818 | 2.568 | 2.022 | 1.714 | 1.339 | 1.206 | 1.050 | 0.877 | 0.733 |
| 160 | - | 2.875 | 2.875 | 2.061 | 1.750 | 1.369 | 1.232 | 1.072 | 0.896 | 0.751 |
| 165 | - | 3.183 | 3.183 | 2.101 | 1.787 | 1.400 | 1.258 | 1.094 | 0.916 | 0.770 |
| 170 | - | 3.491 | 3.491 | 2.140 | 1.823 | 1.431 | 1.284 | 1.115 | 0.936 | 0.789 |
| 175 | - | 3.798 | 3.798 | 2.179 | 1.859 | 1.461 | 1.310 | 1.137 | 0.956 | 0.808 |
| 180 | - | - | - | 2.218 | 1.895 | 1.492 | 1.336 | 1.158 | 0.976 | 0.826 |
| 185 | - | - | - | 2.257 | 1.932 | 1.522 | 1.362 | 1.180 | 0.995 | 0.845 |
| 190 | - | - | - | 2.296 | 1.968 | 1.553 | 1.388 | 1.201 | 1.015 | 0.864 |
| 195 | - | - | - | 2.354 | 2.004 | 1.583 | 1.414 | 1.223 | 1.035 | 0.883 |
| 200 | - | - | - | 2.475 | 2.041 | 1.614 | 1.440 | 1.245 | 1.055 | 0.901 |
| 205 | - | - | - | 2.596 | 2.077 | 1.645 | 1.466 | 1.266 | 1.075 | 0.920 |
| 210 | - | - | - | 2.717 | 2.113 | 1.675 | 1.492 | 1.288 | 1.094 | 0.939 |
| 215 | - | - | - | 2.839 | 2.149 | 1.706 | 1.518 | 1.309 | 1.114 | 0.958 |
| 220 | - | - | - | 2.960 | 2.186 | 1.739 | 1.544 | 1.331 | 1.134 | 0.976 |
| 225 | - | - | - | 3.081 | 2.222 | 1.773 | 1.570 | 1.353 | 1.154 | 0.995 |
| 230 | - | - | - | 3.202 | 2.258 | 1.807 | 1.596 | 1.374 | 1.173 | 1.014 |
| 235 | - | - | - | 3.323 | 2.295 | 1.841 | 1.622 | 1.396 | 1.193 | 1.032 |
| 240 | - | - | - | 3.444 | 2.342 | 1.874 | 1.648 | 1.417 | 1.213 | 1.051 |
| 245 | - | - | - | 3.565 | 2.460 | 1.908 | 1.674 | 1.439 | 1.233 | 1.070 |
| 250 | - | - | - | 3.686 | 2.579 | 1.942 | 1.700 | 1.461 | 1.253 | 1.089 |
| 255 | - | - | - | 3.807 | 2.697 | 1.976 | 1.731 | 1.482 | 1.272 | 1.107 |
| 260 | - | - | - | - | 2.816 | 2.010 | 1.767 | 1.504 | 1.292 | 1.126 |
| 265 | - | - | - | - | 2.934 | 2.044 | 1.804 | 1.525 | 1.312 | 1.145 |
| 270 | - | - | - | - | 3.052 | 2.078 | 1.840 | 1.547 | 1.332 | 1.164 |
| 275 | - | - | - | - | 3.171 | 2.112 | 1.877 | 1.569 | 1.352 | 1.182 |
| 280 | - | - | - | - | 3.289 | 2.146 | 1.913 | 1.590 | 1.371 | 1.201 |
| 285 | - | - | - | - | 3.408 | 2.179 | 1.950 | 1.612 | 1.391 | 1.220 |
| 290 | - | - | - | - | 3.526 | 2.213 | 1.986 | 1.633 | 1.411 | 1.239 |
| 295 | - | - | - | - | 3.645 | 2.247 | 2.023 | 1.655 | 1.431 | 1.257 |
| 300 | - | - | - | - | 3.763 | 2.281 | 2.059 | 1.676 | 1.451 | 1.276 |
| 305 | - | - | - | - | 3.882 | 2.315 | 2.096 | 1.698 | 1.470 | 1.295 |
| 310 | - | - | - | - | 2.495 | 2.132 | 1.733 | 1.490 | 1.313 | |
| 315 | - | - | - | - | 2.745 | 2.169 | 1.793 | 1.510 | 1.332 | |
| 320 | - | - | - | - | 2.996 | 2.205 | 1.853 | 1.530 | 1.351 | |
| 325 | - | - | - | - | 3.246 | 2.242 | 1.913 | 1.550 | 1.370 | |
| 330 | - | - | - | - | 3.496 | 2.278 | 1.973 | 1.569 | 1.388 | |
| 335 | - | - | - | - | 3.746 | 2.315 | 2.033 | 1.589 | 1.407 | |
| 340 | - | - | - | - | - | 2.670 | 2.093 | 1.609 | 1.426 | |
| 345 | - | - | - | - | - | 3.163 | 2.153 | 1.629 | 1.445 | |
| 350 | - | - | - | - | - | 3.655 | 2.213 | 1.649 | 1.463 | |
| 355 | - | - | - | - | - | - | 2.273 | 1.668 | 1.482 | |
| 360 | - | - | - | - | - | - | 2.389 | 1.688 | 1.501 | |
| 365 | - | - | - | - | - | - | 2.939 | 1.708 | 1.520 | |

Thickness is intumescent only.

Results apply to I/H-section beams with concrete slabs with 3 sided fire exposure.

Table 6: I/H-Beam Sections 105 Minutes

| Section Factor up to m ⁻¹ | Thickness (mm) Required for a Design Temperature of | | | | | | | | | |
|--------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 620°C | 650°C | 700°C | 750°C |
| 30 | - | - | 2.102 | 1.805 | 1.493 | 1.242 | 1.154 | 1.036 | 0.869 | 0.711 |
| 35 | - | - | 2.102 | 1.805 | 1.493 | 1.242 | 1.154 | 1.036 | 0.869 | 0.711 |
| 40 | - | - | 2.102 | 1.805 | 1.493 | 1.242 | 1.154 | 1.036 | 0.869 | 0.711 |
| 45 | - | - | 2.102 | 1.805 | 1.493 | 1.242 | 1.154 | 1.036 | 0.869 | 0.711 |
| 50 | - | - | 2.102 | 1.805 | 1.493 | 1.242 | 1.154 | 1.036 | 0.869 | 0.711 |
| 55 | - | - | 2.102 | 1.805 | 1.493 | 1.242 | 1.154 | 1.036 | 0.869 | 0.711 |
| 60 | - | - | 2.102 | 1.805 | 1.493 | 1.242 | 1.154 | 1.036 | 0.869 | 0.711 |
| 65 | - | - | 2.102 | 1.805 | 1.493 | 1.242 | 1.154 | 1.036 | 0.869 | 0.711 |
| 70 | - | - | 2.102 | 1.805 | 1.493 | 1.242 | 1.154 | 1.036 | 0.869 | 0.711 |
| 75 | - | - | 2.102 | 1.805 | 1.493 | 1.242 | 1.154 | 1.036 | 0.869 | 0.711 |
| 80 | - | - | 2.102 | 1.805 | 1.493 | 1.242 | 1.154 | 1.036 | 0.869 | 0.711 |
| 85 | - | - | 2.102 | 1.805 | 1.493 | 1.242 | 1.154 | 1.036 | 0.869 | 0.711 |
| 90 | - | - | 2.102 | 1.805 | 1.493 | 1.242 | 1.154 | 1.036 | 0.869 | 0.711 |
| 95 | - | - | 2.167 | 1.859 | 1.556 | 1.290 | 1.197 | 1.071 | 0.893 | 0.731 |
| 100 | - | - | 2.233 | 1.913 | 1.618 | 1.337 | 1.239 | 1.106 | 0.917 | 0.750 |
| 105 | - | - | 2.298 | 1.967 | 1.681 | 1.385 | 1.281 | 1.140 | 0.941 | 0.770 |
| 110 | - | - | 2.364 | 2.020 | 1.799 | 1.432 | 1.323 | 1.175 | 0.965 | 0.789 |
| 115 | - | - | 2.429 | 2.074 | 1.974 | 1.480 | 1.365 | 1.210 | 0.989 | 0.809 |
| 120 | - | - | 2.495 | 2.149 | 2.149 | 1.527 | 1.407 | 1.244 | 1.013 | 0.828 |
| 125 | - | - | 2.560 | 2.324 | 2.324 | 1.575 | 1.450 | 1.279 | 1.037 | 0.848 |
| 130 | - | - | 2.626 | 2.499 | 2.499 | 1.622 | 1.492 | 1.314 | 1.061 | 0.867 |
| 135 | - | - | 2.691 | 2.674 | 2.674 | 1.670 | 1.534 | 1.348 | 1.085 | 0.887 |
| 140 | - | - | 2.849 | 2.849 | 2.849 | 1.716 | 1.576 | 1.383 | 1.109 | 0.906 |
| 145 | - | - | 3.024 | 3.024 | 3.024 | 1.755 | 1.618 | 1.418 | 1.133 | 0.926 |
| 150 | - | - | 3.198 | 3.198 | 3.198 | 1.794 | 1.660 | 1.453 | 1.157 | 0.946 |
| 155 | - | - | 3.373 | 3.373 | 3.373 | 1.832 | 1.702 | 1.487 | 1.181 | 0.965 |
| 160 | - | - | 3.548 | 3.548 | 3.548 | 1.871 | 1.741 | 1.522 | 1.205 | 0.985 |
| 165 | - | - | 3.723 | 3.723 | 3.723 | 1.909 | 1.778 | 1.557 | 1.229 | 1.004 |
| 170 | - | - | 3.898 | 3.898 | 3.898 | 1.948 | 1.816 | 1.591 | 1.253 | 1.024 |
| 175 | - | - | - | - | - | 1.987 | 1.853 | 1.626 | 1.277 | 1.043 |
| 180 | - | - | - | - | - | 2.025 | 1.890 | 1.661 | 1.301 | 1.063 |
| 185 | - | - | - | - | - | 2.064 | 1.928 | 1.695 | 1.325 | 1.082 |
| 190 | - | - | - | - | - | 2.103 | 1.965 | 1.731 | 1.349 | 1.102 |
| 195 | - | - | - | - | - | 2.141 | 2.003 | 1.767 | 1.373 | 1.121 |
| 200 | - | - | - | - | - | 2.180 | 2.040 | 1.803 | 1.397 | 1.141 |
| 205 | - | - | - | - | - | 2.219 | 2.077 | 1.839 | 1.421 | 1.160 |
| 210 | - | - | - | - | - | 2.257 | 2.115 | 1.875 | 1.445 | 1.180 |
| 215 | - | - | - | - | - | 2.296 | 2.152 | 1.911 | 1.469 | 1.200 |
| 220 | - | - | - | - | - | 2.365 | 2.190 | 1.947 | 1.493 | 1.219 |
| 225 | - | - | - | - | - | 2.542 | 2.227 | 1.983 | 1.517 | 1.239 |
| 230 | - | - | - | - | - | 2.718 | 2.264 | 2.019 | 1.541 | 1.258 |
| 235 | - | - | - | - | - | 2.895 | 2.302 | 2.055 | 1.565 | 1.278 |
| 240 | - | - | - | - | - | 3.072 | 2.376 | 2.091 | 1.589 | 1.297 |
| 245 | - | - | - | - | - | 3.248 | 2.518 | 2.127 | 1.613 | 1.317 |
| 250 | - | - | - | - | - | 3.425 | 2.660 | 2.164 | 1.637 | 1.336 |
| 255 | - | - | - | - | - | 3.602 | 2.801 | 2.200 | 1.661 | 1.356 |
| 260 | - | - | - | - | - | 3.779 | 2.943 | 2.236 | 1.685 | 1.375 |
| 265 | - | - | - | - | - | - | 3.085 | 2.272 | 1.709 | 1.395 |
| 270 | - | - | - | - | - | - | 3.227 | 2.308 | 1.750 | 1.414 |
| 275 | - | - | - | - | - | - | 3.369 | 2.423 | 1.793 | 1.434 |
| 280 | - | - | - | - | - | - | 3.511 | 2.620 | 1.837 | 1.454 |
| 285 | - | - | - | - | - | - | 3.653 | 2.817 | 1.880 | 1.473 |
| 290 | - | - | - | - | - | - | 3.795 | 3.014 | 1.924 | 1.493 |
| 295 | - | - | - | - | - | - | - | 3.211 | 1.967 | 1.512 |
| 300 | - | - | - | - | - | - | - | 3.408 | 2.011 | 1.532 |
| 305 | - | - | - | - | - | - | - | 3.605 | 2.054 | 1.551 |
| 310 | - | - | - | - | - | - | - | 3.802 | 2.098 | 1.571 |
| 315 | - | - | - | - | - | - | - | - | 2.141 | 1.590 |
| 320 | - | - | - | - | - | - | - | - | 2.185 | 1.610 |
| 325 | - | - | - | - | - | - | - | - | 2.228 | 1.629 |
| 330 | - | - | - | - | - | - | - | - | 2.272 | 1.649 |
| 335 | - | - | - | - | - | - | - | - | 2.315 | 1.669 |
| 340 | - | - | - | - | - | - | - | - | 2.832 | 1.688 |
| 345 | - | - | - | - | - | - | - | - | 3.505 | 1.708 |
| 350 | - | - | - | - | - | - | - | - | - | 1.799 |
| 355 | - | - | - | - | - | - | - | - | - | 1.911 |
| 360 | - | - | - | - | - | - | - | - | - | 2.023 |
| 365 | - | - | - | - | - | - | - | - | - | 2.134 |

Thickness is intumescent only.

Results apply to I/H-section beams with concrete slabs with 3 sided fire exposure.

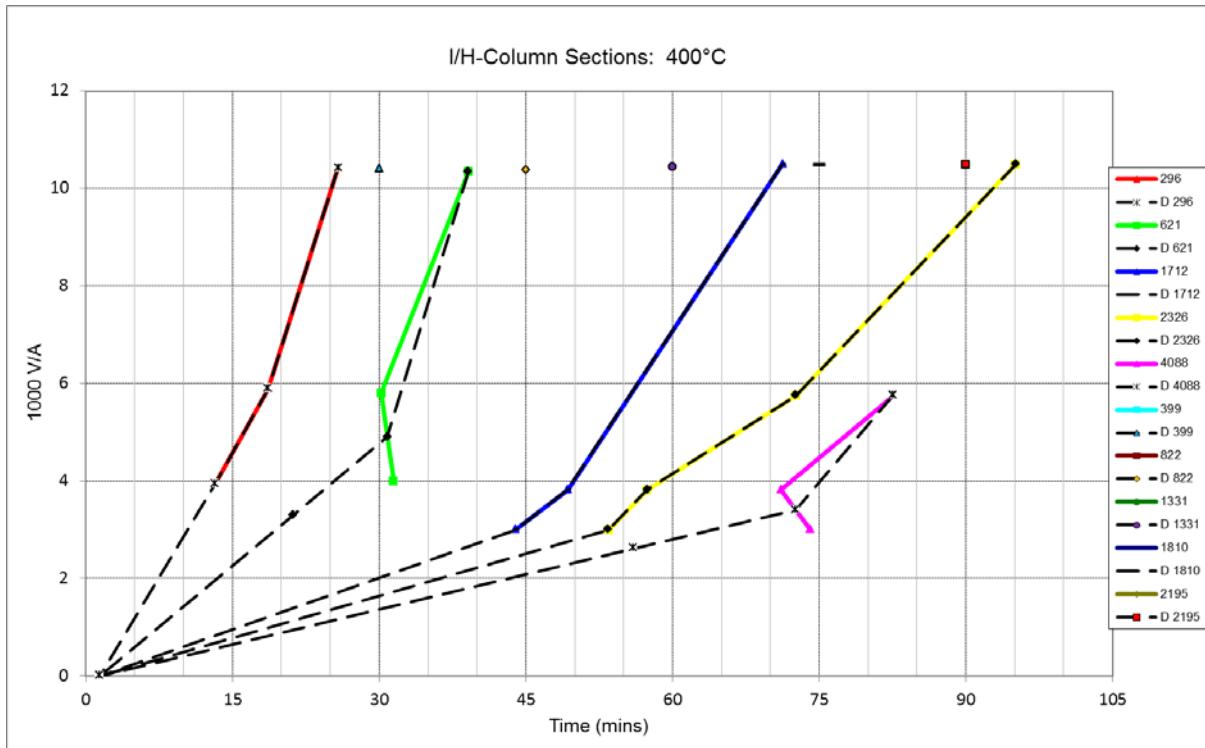
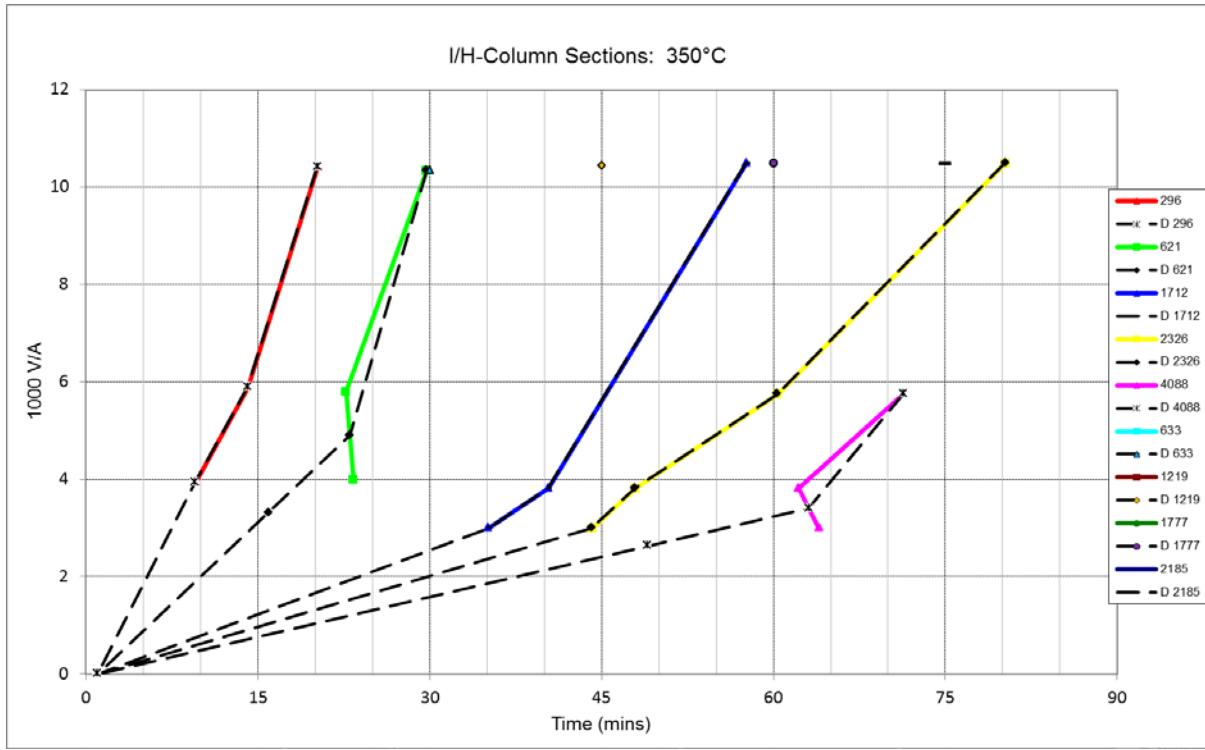
| Section Factor up to m ⁻¹ | Table 7: I/H-Beam Sections 120 Minutes | | | | | | | | | |
|--------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | Thickness (mm) Required for a Design Temperature of | | | | | | | | | |
| | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 620°C | 650°C | 700°C | 750°C |
| 30 | - | - | - | 2.190 | 1.835 | 1.443 | 1.443 | 1.301 | 1.108 | 0.941 |
| 35 | - | - | - | 2.190 | 1.835 | 1.443 | 1.443 | 1.301 | 1.108 | 0.941 |
| 40 | - | - | - | 2.190 | 1.835 | 1.443 | 1.443 | 1.301 | 1.108 | 0.941 |
| 45 | - | - | - | 2.190 | 1.835 | 1.443 | 1.443 | 1.301 | 1.108 | 0.941 |
| 50 | - | - | - | 2.190 | 1.835 | 1.443 | 1.443 | 1.301 | 1.108 | 0.941 |
| 55 | - | - | - | 2.190 | 1.835 | 1.443 | 1.443 | 1.301 | 1.108 | 0.941 |
| 60 | - | - | - | 2.190 | 1.835 | 1.443 | 1.443 | 1.301 | 1.108 | 0.941 |
| 65 | - | - | - | 2.190 | 1.835 | 1.443 | 1.443 | 1.301 | 1.108 | 0.941 |
| 70 | - | - | - | 2.190 | 1.835 | 1.443 | 1.443 | 1.301 | 1.108 | 0.941 |
| 75 | - | - | - | 2.190 | 1.835 | 1.443 | 1.443 | 1.301 | 1.108 | 0.941 |
| 80 | - | - | - | 2.190 | 1.835 | 1.443 | 1.443 | 1.301 | 1.108 | 0.941 |
| 85 | - | - | - | 2.190 | 1.835 | 1.443 | 1.443 | 1.301 | 1.108 | 0.941 |
| 90 | - | - | - | 2.190 | 1.835 | 1.443 | 1.443 | 1.301 | 1.108 | 0.941 |
| 95 | - | - | - | 2.266 | 1.895 | 1.501 | 1.501 | 1.351 | 1.145 | 0.968 |
| 100 | - | - | - | 2.343 | 1.955 | 1.615 | 1.560 | 1.401 | 1.182 | 0.995 |
| 105 | - | - | - | 2.419 | 2.015 | 1.731 | 1.618 | 1.451 | 1.220 | 1.022 |
| 110 | - | - | - | 2.496 | 2.075 | 1.779 | 1.677 | 1.500 | 1.257 | 1.049 |
| 115 | - | - | - | 2.572 | 2.135 | 1.826 | 1.729 | 1.550 | 1.294 | 1.076 |
| 120 | - | - | - | 2.649 | 2.195 | 1.873 | 1.773 | 1.600 | 1.332 | 1.103 |
| 125 | - | - | - | 2.725 | 2.255 | 1.920 | 1.817 | 1.650 | 1.369 | 1.130 |
| 130 | - | - | - | 2.802 | 2.315 | 1.968 | 1.861 | 1.699 | 1.406 | 1.157 |
| 135 | - | - | - | 2.878 | 2.375 | 2.015 | 1.905 | 1.743 | 1.444 | 1.184 |
| 140 | - | - | - | 2.955 | 2.435 | 2.062 | 1.949 | 1.785 | 1.481 | 1.211 |
| 145 | - | - | - | 3.031 | 2.495 | 2.110 | 1.993 | 1.826 | 1.518 | 1.238 |
| 150 | - | - | - | 3.108 | 2.555 | 2.157 | 2.037 | 1.868 | 1.556 | 1.265 |
| 155 | - | - | - | 3.184 | 2.615 | 2.204 | 2.081 | 1.909 | 1.593 | 1.292 |
| 160 | - | - | - | 3.261 | 2.675 | 2.251 | 2.125 | 1.951 | 1.630 | 1.319 |
| 165 | - | - | - | 3.337 | 2.735 | 2.299 | 2.169 | 1.993 | 1.668 | 1.346 |
| 170 | - | - | - | 3.414 | 2.795 | 2.346 | 2.213 | 2.034 | 1.705 | 1.373 |
| 175 | - | - | - | 3.490 | 2.855 | 2.393 | 2.257 | 2.076 | 1.742 | 1.400 |
| 180 | - | - | - | 3.567 | 2.915 | 2.440 | 2.301 | 2.117 | 1.780 | 1.427 |
| 185 | - | - | - | 3.643 | 2.975 | 2.488 | 2.345 | 2.159 | 1.818 | 1.454 |
| 190 | - | - | - | 3.720 | 3.035 | 2.535 | 2.389 | 2.201 | 1.855 | 1.481 |
| 195 | - | - | - | 3.796 | 3.095 | 2.582 | 2.433 | 2.242 | 1.893 | 1.508 |
| 200 | - | - | - | 3.873 | 3.154 | 2.629 | 2.477 | 2.284 | 1.930 | 1.535 |
| 205 | - | - | - | - | 3.214 | 2.677 | 2.521 | 2.325 | 1.968 | 1.562 |
| 210 | - | - | - | - | 3.274 | 2.724 | 2.565 | 2.367 | 2.006 | 1.589 |
| 215 | - | - | - | - | 3.334 | 2.771 | 2.609 | 2.408 | 2.043 | 1.616 |
| 220 | - | - | - | - | 3.394 | 2.819 | 2.653 | 2.450 | 2.081 | 1.643 |
| 225 | - | - | - | - | 3.454 | 2.866 | 2.697 | 2.492 | 2.118 | 1.670 |
| 230 | - | - | - | - | 3.514 | 2.913 | 2.741 | 2.533 | 2.156 | 1.697 |
| 235 | - | - | - | - | 3.574 | 2.960 | 2.785 | 2.575 | 2.193 | 1.731 |
| 240 | - | - | - | - | 3.634 | 3.008 | 2.829 | 2.616 | 2.231 | 1.774 |
| 245 | - | - | - | - | 3.694 | 3.055 | 2.873 | 2.658 | 2.269 | 1.817 |
| 250 | - | - | - | - | 3.754 | 3.102 | 2.917 | 2.700 | 2.306 | 1.860 |
| 255 | - | - | - | - | 3.814 | 3.149 | 2.961 | 2.741 | 2.412 | 1.903 |
| 260 | - | - | - | - | 3.874 | 3.197 | 3.005 | 2.783 | 2.594 | 1.946 |
| 265 | - | - | - | - | - | 3.244 | 3.049 | 2.824 | 2.776 | 1.989 |
| 270 | - | - | - | - | - | 3.291 | 3.093 | 2.958 | 2.958 | 2.032 |
| 275 | - | - | - | - | - | 3.339 | 3.140 | 3.140 | 3.140 | 2.075 |
| 280 | - | - | - | - | - | 3.386 | 3.322 | 3.322 | 3.322 | 2.118 |
| 285 | - | - | - | - | - | 3.504 | 3.504 | 3.504 | 3.504 | 2.161 |
| 290 | - | - | - | - | - | 3.686 | 3.686 | 3.686 | 3.686 | 2.204 |
| 295 | - | - | - | - | - | 3.868 | 3.868 | 3.868 | 3.868 | 2.246 |
| 300 | - | - | - | - | - | - | - | - | - | 2.289 |
| 305 | - | - | - | - | - | - | - | - | - | 2.378 |
| 310 | - | - | - | - | - | - | - | - | - | 2.726 |
| 315 | - | - | - | - | - | - | - | - | - | 3.073 |
| 320 | - | - | - | - | - | - | - | - | - | 3.421 |
| 325 | - | - | - | - | - | - | - | - | - | 3.768 |
| 330 | - | - | - | - | - | - | - | - | - | - |
| 335 | - | - | - | - | - | - | - | - | - | - |
| 340 | - | - | - | - | - | - | - | - | - | - |
| 345 | - | - | - | - | - | - | - | - | - | - |
| 350 | - | - | - | - | - | - | - | - | - | - |
| 355 | - | - | - | - | - | - | - | - | - | - |
| 360 | - | - | - | - | - | - | - | - | - | - |
| 365 | - | - | - | - | - | - | - | - | - | - |

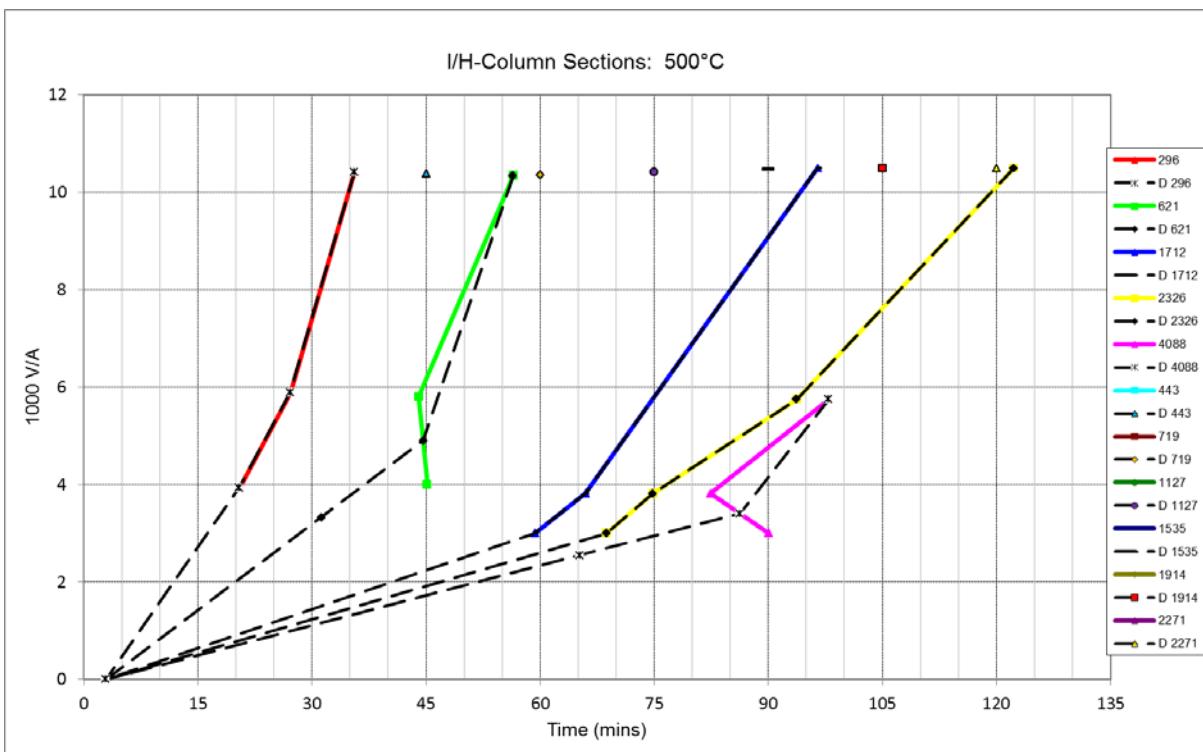
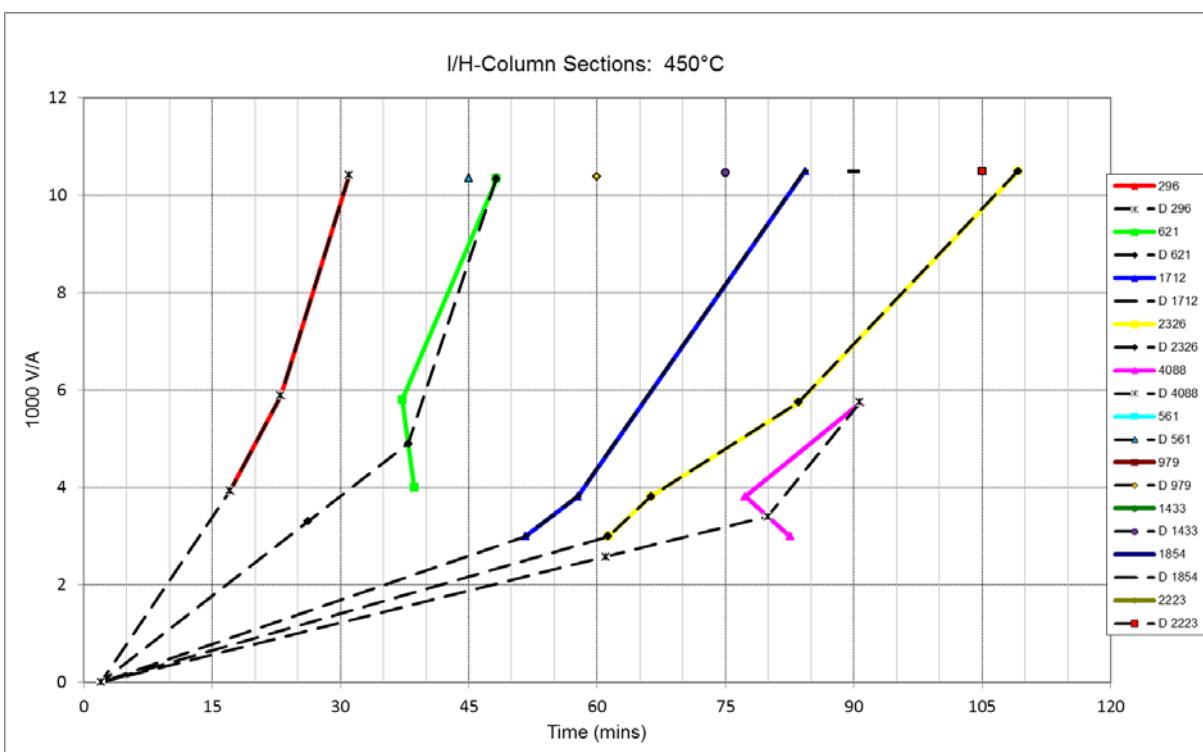
Thickness is intumescent only.

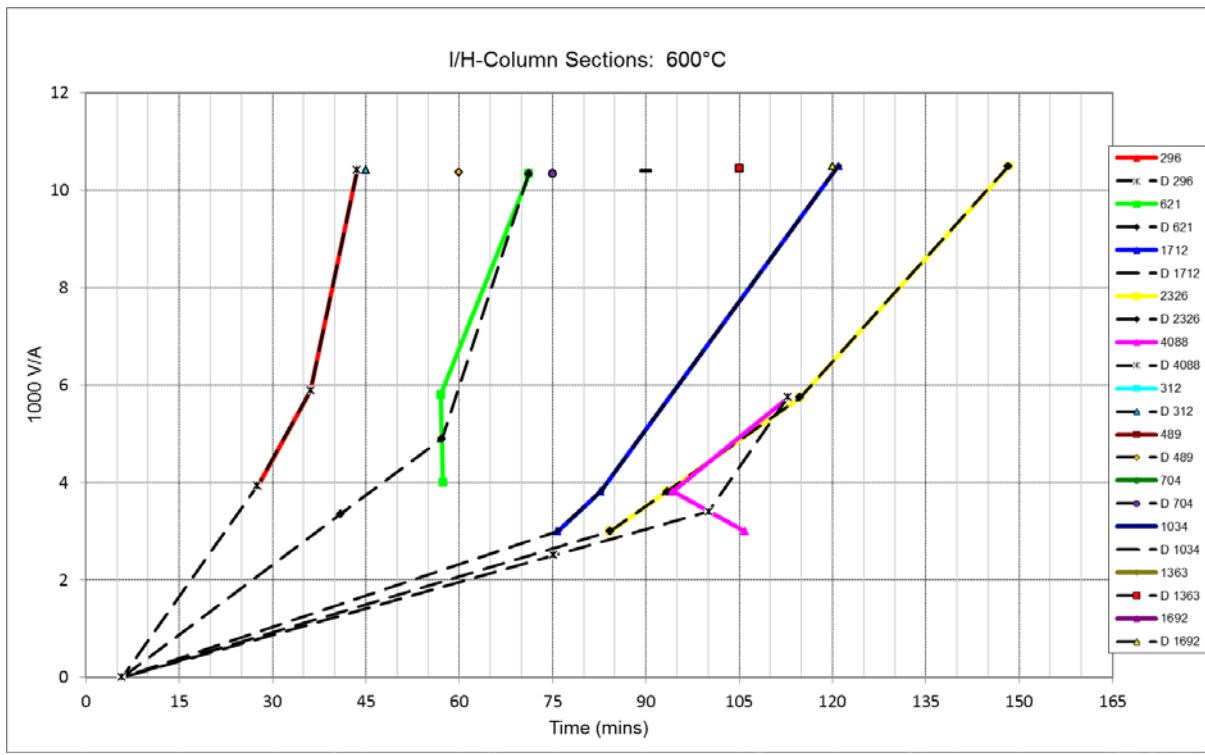
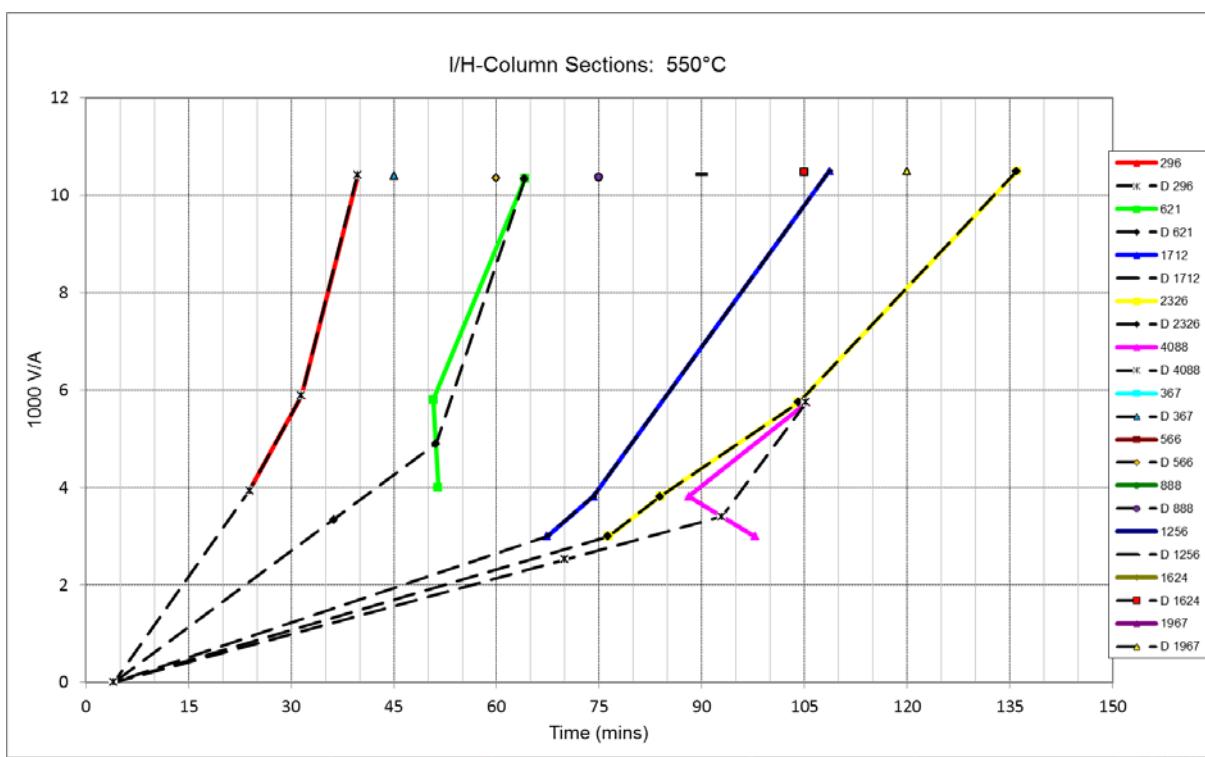
Results apply to I/H-section beams with concrete slabs with 3 sided fire exposure.

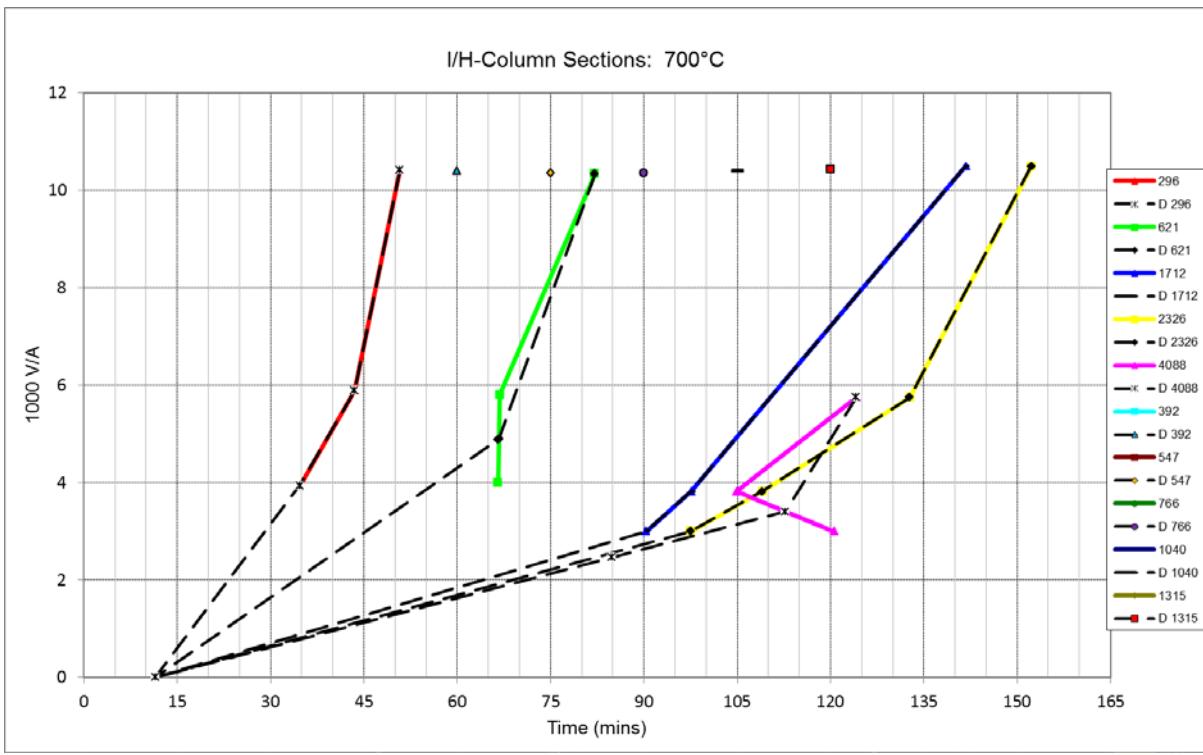
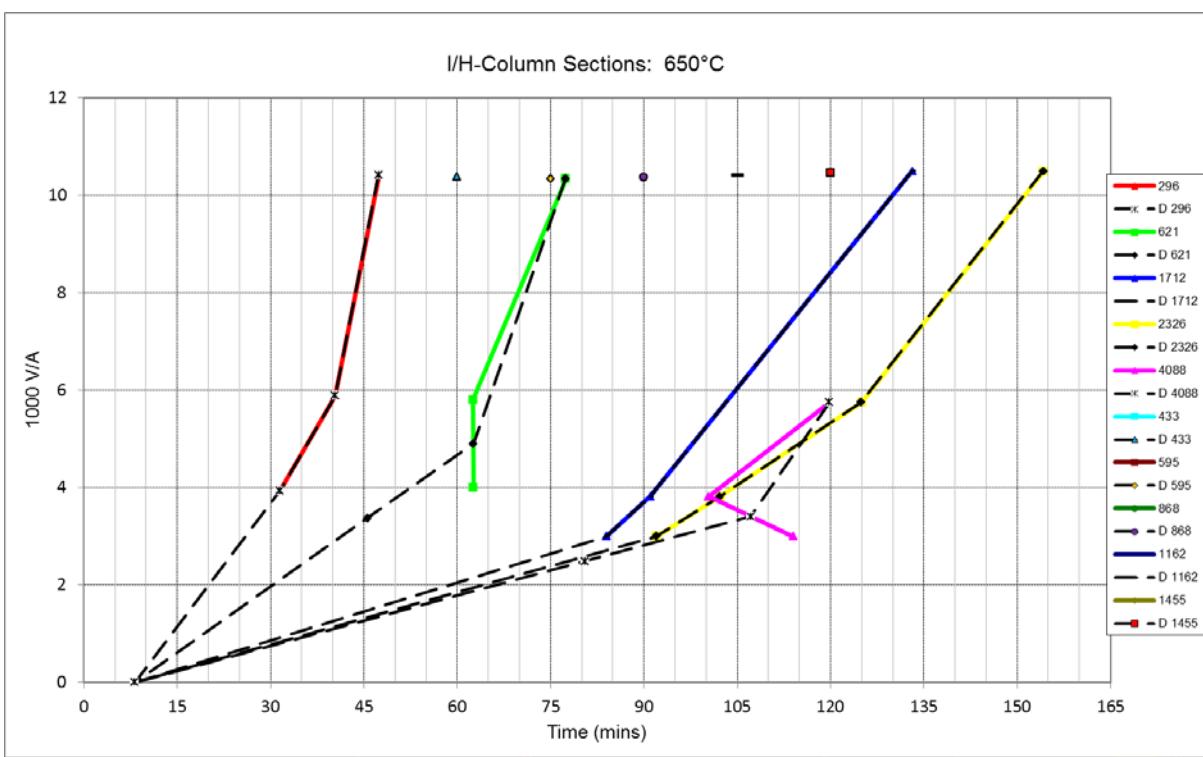
Annex B: I/H-section Columns

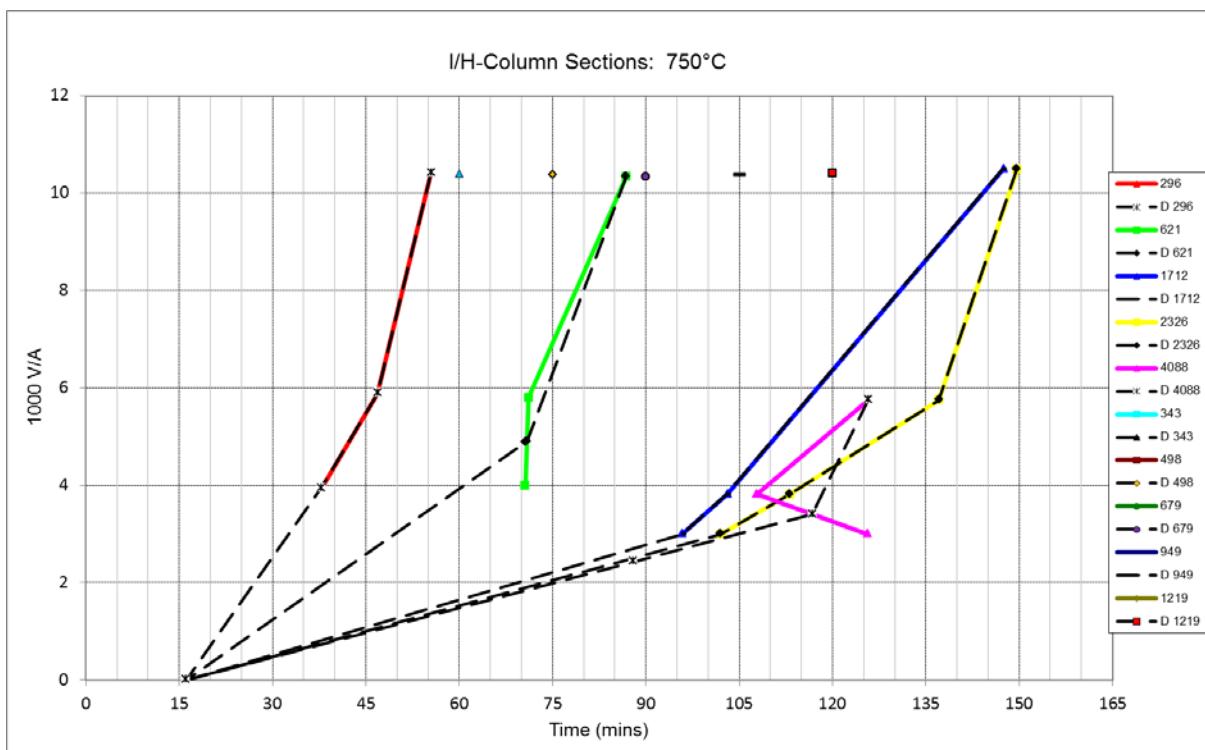
B1 Graphs: I/H-section Columns











B2 Criteria of Acceptability/Intercepts: I/H-section Columns

B2.1 Criteria of Acceptability

| Acceptability Criteria | % Allowed / Actual | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 650°C | 700°C | 750°C |
|--------------------------------|--------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Maximum positive variation (%) | 15 | 1.44 | 2.11 | 3.41 | 4.68 | 5.48 | 6.15 | 6.75 | 7.46 | 8.27 |
| Optimistic predictions (%) | 30 | 12.50 | 12.50 | 12.50 | 12.50 | 12.50 | 12.50 | 12.50 | 12.50 | 12.50 |
| Overall conservative (%) | less than zero | -3.43 | -3.37 | -3.38 | -3.37 | -3.32 | -3.25 | -3.15 | -1.45 | -1.41 |

B2.2 Intercepts

| Dry Film Thickness (mm) | I/H-Column Sections: Limiting section factor m-1 at design temperature 350°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | - | - | - | - | - | - | - |
| 0.621 | - | - | - | - | - | - | - |
| 0.633 | 96.8 | - | - | - | - | - | - |
| 1.219 | - | 96.0 | - | - | - | - | - |
| 1.712 | 392.9 | 177.6 | - | - | - | - | - |
| 1.777 | - | - | 95.3 | - | - | - | - |
| 2.185 | - | - | - | 95.3 | - | - | - |
| 2.326 | 496.5 | 313.7 | 175.3 | 108.1 | - | - | - |
| 4.088 | 628.7 | 414.4 | 309.0 | - | - | - | - |

| Dry Film Thickness (mm) | I/H-Column Sections: Limiting section factor m-1 at design temperature 400°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | - | - | - | - | - | - | - |
| 0.399 | 96.3 | - | - | - | - | - | - |
| 0.621 | 210.1 | - | - | - | - | - | - |
| 0.822 | - | 96.5 | - | - | - | - | - |
| 1.331 | - | - | 95.8 | - | - | - | - |
| 1.712 | 496.5 | 316.1 | 141.0 | - | - | - | - |
| 1.810 | - | - | - | 95.3 | - | - | - |
| 2.195 | - | - | - | - | 95.3 | - | - |
| 2.326 | 607.5 | 398.5 | 241.2 | 159.8 | 106.2 | - | - |
| 4.088 | 731.2 | 479.6 | 356.9 | 251.6 | - | - | - |

| Dry Film Thickness (mm) | I/H-Column Sections: Limiting section factor m-1 at design temperature 450°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 101.5 | - | - | - | - | - | - |
| 0.561 | - | 96.7 | - | - | - | - | - |
| 0.621 | 261.9 | 115.8 | - | - | - | - | - |
| 0.979 | - | - | 96.3 | - | - | - | - |
| 1.433 | - | - | - | 95.7 | - | - | - |
| 1.712 | 591.8 | 385.4 | 227.5 | 122.3 | - | - | - |
| 1.854 | - | - | - | - | 95.3 | - | - |
| 2.223 | - | - | - | - | - | 95.3 | - |
| 2.326 | 707.6 | 460.7 | 341.6 | 208.6 | 143.9 | 102.9 | - |
| 4.088 | 817.6 | 532.4 | 394.7 | 313.6 | 178.6 | - | - |

| Dry Film Thickness (mm) | I/H-Column Sections: Limiting section factor m-1 at design temperature 500°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 134.6 | - | - | - | - | - | - |
| 0.443 | - | 96.4 | - | - | - | - | - |
| 0.621 | 314.2 | 197.0 | - | - | - | - | - |
| 0.719 | - | - | 96.7 | - | - | - | - |
| 1.127 | - | - | - | 96.1 | - | - | - |
| 1.535 | - | - | - | - | 95.5 | - | - |
| 1.712 | 694.1 | 446.8 | 323.5 | 172.4 | 110.2 | - | - |
| 1.914 | - | - | - | - | - | 95.3 | - |
| 2.271 | - | - | - | - | - | - | 95.3 |
| 2.326 | 811.2 | 522.2 | 385.0 | 260.7 | 186.2 | 131.2 | 98.9 |
| 4.088 | 903.5 | 581.6 | 428.8 | 339.6 | 240.5 | - | - |

| Dry Film Thickness (mm) | I/H-Column Sections: Limiting section factor m-1 at design temperature 550°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 181.9 | - | - | - | - | - | - |
| 0.367 | - | 96.2 | - | - | - | - | - |
| 0.566 | - | - | 96.7 | - | - | - | - |
| 0.621 | 370.8 | 234.8 | 116.1 | - | - | - | - |
| 0.888 | - | - | - | 96.4 | - | - | - |
| 1.256 | - | - | - | - | 95.9 | - | - |
| 1.624 | - | - | - | - | - | 95.4 | - |
| 1.712 | 815.3 | 516.3 | 377.7 | 250.7 | 145.1 | 102.1 | - |
| 1.967 | - | - | - | - | - | - | 95.3 |
| 2.326 | 931.4 | 589.8 | 431.5 | 340.2 | 227.3 | 169.9 | 123.2 |
| 4.088 | 1007.5 | 638.0 | 466.8 | 368.0 | 303.8 | 175.1 | - |

| Dry Film Thickness (mm) | I/H-Column Sections: Limiting section factor m-1 at design temperature 600°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 222.9 | - | - | - | - | - | - |
| 0.312 | - | 96.0 | - | - | - | - | - |
| 0.489 | - | - | 96.5 | - | - | - | - |
| 0.621 | 433.7 | 267.8 | 167.3 | - | - | - | - |
| 0.704 | - | - | - | 96.7 | - | - | - |
| 1.034 | - | - | - | - | 96.2 | - | - |
| 1.363 | - | - | - | - | - | 95.8 | - |
| 1.692 | - | - | - | - | - | - | 95.3 |
| 1.712 | 965.0 | 595.8 | 430.9 | 337.5 | 196.4 | 129.6 | 96.8 |
| 2.326 | 1082.4 | 668.2 | 483.3 | 378.5 | 284.8 | 205.6 | 154.2 |
| 4.088 | 1144.9 | 706.8 | 511.2 | 400.4 | 329.1 | 232.2 | - |

| Dry Film Thickness (mm) | I/H-Column Sections: Limiting section factor m-1 at design temperature 650°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 271.5 | 112.8 | - | - | - | - | - |
| 0.433 | - | - | 96.3 | - | - | - | - |
| 0.595 | - | - | - | 96.7 | - | - | - |
| 0.621 | 509.3 | 301.7 | 214.4 | 105.8 | - | - | - |
| 0.868 | - | - | - | - | 96.5 | - | - |
| 1.162 | - | - | - | - | - | 96.1 | - |
| 1.455 | - | - | - | - | - | - | 95.6 |
| 1.712 | 1160.2 | 687.3 | 488.3 | 378.6 | 270.3 | 165.7 | 118.8 |
| 2.326 | 1284.3 | 760.8 | 540.5 | 419.1 | 342.3 | 246.7 | 187.5 |
| 4.088 | 1334.0 | 790.3 | 561.4 | 435.4 | 355.5 | 300.4 | - |

| Dry Film Thickness (mm) | I/H-Column Sections: Limiting section factor m-1 at design temperature 700°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 318.5 | 146.8 | - | - | - | - | - |
| 0.392 | - | - | 96.2 | - | - | - | - |
| 0.547 | - | - | - | 96.6 | - | - | - |
| 0.621 | 609.2 | 336.4 | 232.4 | 127.8 | - | - | - |
| 0.766 | - | - | - | - | 96.6 | - | - |
| 1.040 | - | - | - | - | - | 96.2 | - |
| 1.315 | - | - | - | - | - | - | 95.8 |
| 1.712 | 1423.1 | 785.9 | 542.8 | 414.6 | 335.4 | 202.6 | 138.7 |
| 2.326 | 1553.1 | 857.7 | 592.4 | 452.5 | 366.0 | 283.3 | 212.2 |
| 4.088 | 1607.9 | 887.9 | 613.3 | 468.4 | 378.9 | 318.1 | 204.0 |

| Dry Film Thickness (mm) | I/H-Column Sections: Limiting section factor m-1 at design temperature 750°C for a time period of: | | | | | | |
|-------------------------|--|------------|------------|------------|------------|-------------|-------------|
| | 30 minutes | 45 minutes | 60 minutes | 75 minutes | 90 minutes | 105 minutes | 120 minutes |
| 0.296 | 396.5 | 182.6 | - | - | - | - | - |
| 0.343 | - | - | 96.1 | - | - | - | - |
| 0.498 | - | - | - | 96.5 | - | - | - |
| 0.621 | 804.5 | 387.0 | 254.7 | 158.7 | - | - | - |
| 0.679 | - | - | - | - | 96.7 | - | - |
| 0.949 | - | - | - | - | - | 96.3 | - |
| 1.219 | - | - | - | - | - | - | 96.0 |
| 1.712 | 1915.7 | 921.4 | 606.6 | 452.1 | 360.3 | 242.9 | 156.9 |
| 2.326 | 2064.7 | 993.1 | 653.7 | 487.3 | 388.4 | 311.0 | 228.7 |
| 4.088 | 2127.0 | 1023.0 | 673.5 | 501.9 | 400.1 | 332.6 | 234.9 |

Assessment limited to a maximum section factor of 368m⁻¹.

B3 Tables: I/H-section Columns

Table 8: I/H-Column Sections 30 Minutes

| Section Factor up to m ⁻¹ | Thickness (mm) Required for a Design Temperature of | | | | | | | | | |
|--------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 650°C | 700°C | 750°C | |
| 30 | 0.609 | 0.386 | 0.273 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 35 | 0.609 | 0.386 | 0.273 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 40 | 0.609 | 0.386 | 0.273 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 45 | 0.609 | 0.386 | 0.273 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 50 | 0.609 | 0.386 | 0.273 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 55 | 0.609 | 0.386 | 0.273 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 60 | 0.609 | 0.386 | 0.273 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 65 | 0.609 | 0.386 | 0.273 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 70 | 0.609 | 0.386 | 0.273 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 75 | 0.609 | 0.386 | 0.273 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 80 | 0.609 | 0.386 | 0.273 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 85 | 0.609 | 0.386 | 0.273 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 90 | 0.609 | 0.386 | 0.273 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 95 | 0.627 | 0.396 | 0.283 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 100 | 0.645 | 0.406 | 0.293 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 105 | 0.663 | 0.416 | 0.303 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 110 | 0.681 | 0.426 | 0.313 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 115 | 0.699 | 0.436 | 0.323 | 0.261 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 120 | 0.718 | 0.445 | 0.333 | 0.270 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 125 | 0.736 | 0.455 | 0.344 | 0.279 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 130 | 0.754 | 0.465 | 0.354 | 0.288 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 135 | 0.772 | 0.475 | 0.364 | 0.297 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 140 | 0.790 | 0.484 | 0.374 | 0.306 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 145 | 0.809 | 0.494 | 0.384 | 0.315 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 150 | 0.827 | 0.504 | 0.394 | 0.324 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 155 | 0.845 | 0.514 | 0.404 | 0.333 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 160 | 0.863 | 0.523 | 0.414 | 0.342 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 165 | 0.882 | 0.533 | 0.425 | 0.351 | 0.265 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 170 | 0.900 | 0.543 | 0.435 | 0.360 | 0.274 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 175 | 0.918 | 0.553 | 0.445 | 0.369 | 0.283 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 180 | 0.936 | 0.562 | 0.455 | 0.378 | 0.292 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 185 | 0.954 | 0.572 | 0.465 | 0.387 | 0.301 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 190 | 0.973 | 0.582 | 0.475 | 0.396 | 0.310 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 195 | 0.991 | 0.592 | 0.485 | 0.405 | 0.319 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 200 | 1.009 | 0.601 | 0.496 | 0.414 | 0.327 | 0.260 | 0.260 | 0.260 | 0.260 | 0.260 |
| 205 | 1.027 | 0.611 | 0.506 | 0.423 | 0.336 | 0.267 | 0.260 | 0.260 | 0.260 | 0.260 |
| 210 | 1.046 | 0.621 | 0.516 | 0.432 | 0.344 | 0.275 | 0.260 | 0.260 | 0.260 | 0.260 |
| 215 | 1.064 | 0.640 | 0.526 | 0.441 | 0.353 | 0.283 | 0.260 | 0.260 | 0.260 | 0.260 |
| 220 | 1.082 | 0.659 | 0.536 | 0.451 | 0.362 | 0.291 | 0.260 | 0.260 | 0.260 | 0.260 |
| 225 | 1.100 | 0.678 | 0.546 | 0.460 | 0.370 | 0.299 | 0.260 | 0.260 | 0.260 | 0.260 |
| 230 | 1.118 | 0.697 | 0.556 | 0.469 | 0.379 | 0.307 | 0.260 | 0.260 | 0.260 | 0.260 |
| 235 | 1.137 | 0.716 | 0.566 | 0.478 | 0.387 | 0.315 | 0.260 | 0.260 | 0.260 | 0.260 |
| 240 | 1.155 | 0.735 | 0.577 | 0.487 | 0.396 | 0.322 | 0.260 | 0.260 | 0.260 | 0.260 |
| 245 | 1.173 | 0.754 | 0.587 | 0.496 | 0.405 | 0.330 | 0.260 | 0.260 | 0.260 | 0.260 |
| 250 | 1.191 | 0.773 | 0.597 | 0.505 | 0.413 | 0.338 | 0.266 | 0.260 | 0.260 | 0.260 |
| 255 | 1.210 | 0.792 | 0.607 | 0.514 | 0.422 | 0.345 | 0.273 | 0.260 | 0.260 | 0.260 |
| 260 | 1.228 | 0.811 | 0.617 | 0.523 | 0.430 | 0.353 | 0.280 | 0.260 | 0.260 | 0.260 |
| 265 | 1.246 | 0.830 | 0.631 | 0.532 | 0.439 | 0.361 | 0.287 | 0.260 | 0.260 | 0.260 |
| 270 | 1.264 | 0.849 | 0.648 | 0.541 | 0.448 | 0.369 | 0.294 | 0.260 | 0.260 | 0.260 |
| 275 | 1.282 | 0.868 | 0.664 | 0.550 | 0.456 | 0.376 | 0.301 | 0.260 | 0.260 | 0.260 |
| 280 | 1.301 | 0.887 | 0.681 | 0.559 | 0.465 | 0.384 | 0.308 | 0.260 | 0.260 | 0.260 |
| 285 | 1.319 | 0.906 | 0.697 | 0.568 | 0.473 | 0.392 | 0.314 | 0.263 | 0.260 | 0.260 |
| 290 | 1.337 | 0.925 | 0.714 | 0.577 | 0.482 | 0.399 | 0.321 | 0.268 | 0.260 | 0.260 |
| 295 | 1.355 | 0.944 | 0.730 | 0.586 | 0.491 | 0.407 | 0.328 | 0.273 | 0.260 | 0.260 |
| 300 | 1.374 | 0.963 | 0.747 | 0.595 | 0.499 | 0.415 | 0.335 | 0.278 | 0.260 | 0.260 |
| 305 | 1.392 | 0.982 | 0.763 | 0.604 | 0.508 | 0.423 | 0.342 | 0.283 | 0.260 | 0.260 |
| 310 | 1.410 | 1.002 | 0.780 | 0.613 | 0.516 | 0.430 | 0.349 | 0.288 | 0.260 | 0.260 |
| 315 | 1.428 | 1.021 | 0.796 | 0.623 | 0.525 | 0.438 | 0.355 | 0.293 | 0.260 | 0.260 |
| 320 | 1.446 | 1.040 | 0.813 | 0.638 | 0.534 | 0.446 | 0.362 | 0.298 | 0.260 | 0.260 |
| 325 | 1.465 | 1.059 | 0.830 | 0.652 | 0.542 | 0.453 | 0.369 | 0.303 | 0.260 | 0.260 |
| 330 | 1.483 | 1.078 | 0.846 | 0.666 | 0.551 | 0.461 | 0.376 | 0.309 | 0.260 | 0.260 |
| 335 | 1.501 | 1.097 | 0.863 | 0.681 | 0.559 | 0.469 | 0.383 | 0.314 | 0.260 | 0.260 |
| 340 | 1.519 | 1.116 | 0.879 | 0.695 | 0.568 | 0.476 | 0.390 | 0.320 | 0.260 | 0.260 |
| 345 | 1.538 | 1.135 | 0.896 | 0.709 | 0.577 | 0.484 | 0.396 | 0.326 | 0.260 | 0.260 |
| 350 | 1.556 | 1.154 | 0.912 | 0.724 | 0.585 | 0.492 | 0.403 | 0.331 | 0.260 | 0.260 |
| 355 | 1.574 | 1.173 | 0.929 | 0.738 | 0.594 | 0.500 | 0.410 | 0.337 | 0.260 | 0.260 |
| 360 | 1.592 | 1.192 | 0.945 | 0.753 | 0.602 | 0.507 | 0.417 | 0.342 | 0.260 | 0.260 |
| 365 | 1.610 | 1.211 | 0.962 | 0.767 | 0.611 | 0.515 | 0.424 | 0.348 | 0.260 | 0.260 |

Thickness is intumescent only.

Results also apply to I/H-section beams exposed on all four sides limited to a maximum protection thickness of 3.906mm.

Table 9: I/H-Column Sections 45 Minutes

| Section Factor up to m ⁻¹ | Thickness (mm) Required for a Design Temperature of | | | | | | | | |
|--------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|
| | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 650°C | 700°C | 750°C |
| 30 | 1.181 | 0.796 | 0.542 | 0.431 | 0.356 | 0.301 | 0.260 | 0.260 | 0.260 |
| 35 | 1.181 | 0.796 | 0.542 | 0.431 | 0.356 | 0.301 | 0.260 | 0.260 | 0.260 |
| 40 | 1.181 | 0.796 | 0.542 | 0.431 | 0.356 | 0.301 | 0.260 | 0.260 | 0.260 |
| 45 | 1.181 | 0.796 | 0.542 | 0.431 | 0.356 | 0.301 | 0.260 | 0.260 | 0.260 |
| 50 | 1.181 | 0.796 | 0.542 | 0.431 | 0.356 | 0.301 | 0.260 | 0.260 | 0.260 |
| 55 | 1.181 | 0.796 | 0.542 | 0.431 | 0.356 | 0.301 | 0.260 | 0.260 | 0.260 |
| 60 | 1.181 | 0.796 | 0.542 | 0.431 | 0.356 | 0.301 | 0.260 | 0.260 | 0.260 |
| 65 | 1.181 | 0.796 | 0.542 | 0.431 | 0.356 | 0.301 | 0.260 | 0.260 | 0.260 |
| 70 | 1.181 | 0.796 | 0.542 | 0.431 | 0.356 | 0.301 | 0.260 | 0.260 | 0.260 |
| 75 | 1.181 | 0.796 | 0.542 | 0.431 | 0.356 | 0.301 | 0.260 | 0.260 | 0.260 |
| 80 | 1.181 | 0.796 | 0.542 | 0.431 | 0.356 | 0.301 | 0.260 | 0.260 | 0.260 |
| 85 | 1.181 | 0.796 | 0.542 | 0.431 | 0.356 | 0.301 | 0.260 | 0.260 | 0.260 |
| 90 | 1.181 | 0.796 | 0.542 | 0.431 | 0.356 | 0.301 | 0.260 | 0.260 | 0.260 |
| 95 | 1.212 | 0.816 | 0.557 | 0.440 | 0.365 | 0.310 | 0.268 | 0.260 | 0.260 |
| 100 | 1.243 | 0.836 | 0.572 | 0.449 | 0.374 | 0.319 | 0.276 | 0.260 | 0.260 |
| 105 | 1.274 | 0.856 | 0.587 | 0.458 | 0.383 | 0.328 | 0.284 | 0.260 | 0.260 |
| 110 | 1.304 | 0.877 | 0.603 | 0.467 | 0.392 | 0.337 | 0.292 | 0.260 | 0.260 |
| 115 | 1.334 | 0.897 | 0.619 | 0.476 | 0.401 | 0.346 | 0.300 | 0.260 | 0.260 |
| 120 | 1.364 | 0.917 | 0.638 | 0.485 | 0.411 | 0.355 | 0.308 | 0.260 | 0.260 |
| 125 | 1.394 | 0.937 | 0.658 | 0.494 | 0.420 | 0.364 | 0.317 | 0.262 | 0.260 |
| 130 | 1.424 | 0.958 | 0.679 | 0.502 | 0.429 | 0.373 | 0.326 | 0.270 | 0.260 |
| 135 | 1.455 | 0.978 | 0.699 | 0.511 | 0.438 | 0.382 | 0.334 | 0.278 | 0.260 |
| 140 | 1.485 | 0.998 | 0.719 | 0.520 | 0.447 | 0.391 | 0.343 | 0.286 | 0.260 |
| 145 | 1.515 | 1.019 | 0.739 | 0.529 | 0.456 | 0.400 | 0.351 | 0.294 | 0.260 |
| 150 | 1.545 | 1.039 | 0.759 | 0.538 | 0.466 | 0.409 | 0.360 | 0.302 | 0.260 |
| 155 | 1.575 | 1.059 | 0.780 | 0.547 | 0.475 | 0.418 | 0.369 | 0.310 | 0.260 |
| 160 | 1.606 | 1.079 | 0.800 | 0.556 | 0.484 | 0.427 | 0.377 | 0.319 | 0.260 |
| 165 | 1.636 | 1.100 | 0.820 | 0.564 | 0.493 | 0.436 | 0.386 | 0.327 | 0.268 |
| 170 | 1.666 | 1.120 | 0.840 | 0.573 | 0.502 | 0.445 | 0.394 | 0.336 | 0.276 |
| 175 | 1.696 | 1.140 | 0.861 | 0.582 | 0.511 | 0.454 | 0.403 | 0.344 | 0.284 |
| 180 | 1.723 | 1.160 | 0.881 | 0.591 | 0.521 | 0.463 | 0.412 | 0.353 | 0.292 |
| 185 | 1.745 | 1.181 | 0.901 | 0.600 | 0.530 | 0.472 | 0.420 | 0.362 | 0.300 |
| 190 | 1.768 | 1.201 | 0.921 | 0.609 | 0.539 | 0.481 | 0.429 | 0.370 | 0.308 |
| 195 | 1.790 | 1.221 | 0.942 | 0.617 | 0.548 | 0.490 | 0.437 | 0.379 | 0.316 |
| 200 | 1.813 | 1.241 | 0.962 | 0.634 | 0.557 | 0.499 | 0.446 | 0.387 | 0.324 |
| 205 | 1.835 | 1.262 | 0.982 | 0.656 | 0.566 | 0.508 | 0.455 | 0.396 | 0.332 |
| 210 | 1.858 | 1.282 | 1.002 | 0.678 | 0.576 | 0.517 | 0.463 | 0.404 | 0.340 |
| 215 | 1.881 | 1.302 | 1.023 | 0.699 | 0.585 | 0.526 | 0.472 | 0.413 | 0.348 |
| 220 | 1.903 | 1.323 | 1.043 | 0.721 | 0.594 | 0.535 | 0.480 | 0.421 | 0.355 |
| 225 | 1.926 | 1.343 | 1.063 | 0.743 | 0.603 | 0.544 | 0.489 | 0.430 | 0.363 |
| 230 | 1.948 | 1.363 | 1.083 | 0.765 | 0.612 | 0.553 | 0.498 | 0.439 | 0.371 |
| 235 | 1.971 | 1.383 | 1.103 | 0.787 | 0.622 | 0.562 | 0.506 | 0.447 | 0.379 |
| 240 | 1.993 | 1.404 | 1.124 | 0.809 | 0.641 | 0.571 | 0.515 | 0.456 | 0.387 |
| 245 | 2.016 | 1.424 | 1.144 | 0.831 | 0.661 | 0.580 | 0.523 | 0.464 | 0.395 |
| 250 | 2.039 | 1.444 | 1.164 | 0.852 | 0.680 | 0.589 | 0.532 | 0.473 | 0.403 |
| 255 | 2.061 | 1.464 | 1.184 | 0.874 | 0.699 | 0.598 | 0.541 | 0.481 | 0.411 |
| 260 | 2.084 | 1.485 | 1.205 | 0.896 | 0.719 | 0.607 | 0.549 | 0.490 | 0.419 |
| 265 | 2.106 | 1.505 | 1.225 | 0.918 | 0.738 | 0.616 | 0.558 | 0.499 | 0.427 |
| 270 | 2.129 | 1.525 | 1.245 | 0.940 | 0.757 | 0.628 | 0.566 | 0.507 | 0.435 |
| 275 | 2.151 | 1.545 | 1.265 | 0.962 | 0.777 | 0.645 | 0.575 | 0.516 | 0.443 |
| 280 | 2.174 | 1.566 | 1.286 | 0.983 | 0.796 | 0.662 | 0.584 | 0.524 | 0.451 |
| 285 | 2.197 | 1.586 | 1.306 | 1.005 | 0.816 | 0.678 | 0.592 | 0.533 | 0.459 |
| 290 | 2.219 | 1.606 | 1.326 | 1.027 | 0.835 | 0.695 | 0.601 | 0.541 | 0.467 |
| 295 | 2.242 | 1.627 | 1.346 | 1.049 | 0.854 | 0.712 | 0.609 | 0.550 | 0.475 |
| 300 | 2.264 | 1.647 | 1.366 | 1.071 | 0.874 | 0.728 | 0.618 | 0.559 | 0.483 |
| 305 | 2.287 | 1.667 | 1.387 | 1.093 | 0.893 | 0.745 | 0.630 | 0.567 | 0.491 |
| 310 | 2.309 | 1.687 | 1.407 | 1.114 | 0.913 | 0.761 | 0.644 | 0.576 | 0.499 |
| 315 | 2.349 | 1.708 | 1.427 | 1.136 | 0.932 | 0.778 | 0.659 | 0.584 | 0.507 |
| 320 | 2.436 | 1.741 | 1.447 | 1.158 | 0.951 | 0.795 | 0.673 | 0.593 | 0.515 |
| 325 | 2.524 | 1.778 | 1.468 | 1.180 | 0.971 | 0.811 | 0.687 | 0.601 | 0.522 |
| 330 | 2.611 | 1.816 | 1.488 | 1.202 | 0.990 | 0.828 | 0.701 | 0.610 | 0.530 |
| 335 | 2.699 | 1.853 | 1.508 | 1.224 | 1.009 | 0.845 | 0.715 | 0.619 | 0.538 |
| 340 | 2.786 | 1.890 | 1.528 | 1.246 | 1.029 | 0.861 | 0.729 | 0.630 | 0.546 |
| 345 | 2.874 | 1.928 | 1.549 | 1.267 | 1.048 | 0.878 | 0.743 | 0.642 | 0.554 |
| 350 | 2.961 | 1.965 | 1.569 | 1.289 | 1.068 | 0.895 | 0.758 | 0.654 | 0.562 |
| 355 | 3.049 | 2.002 | 1.589 | 1.311 | 1.087 | 0.911 | 0.772 | 0.666 | 0.570 |
| 360 | 3.136 | 2.039 | 1.609 | 1.333 | 1.106 | 0.928 | 0.786 | 0.678 | 0.578 |
| 365 | 3.224 | 2.077 | 1.630 | 1.355 | 1.126 | 0.944 | 0.800 | 0.690 | 0.586 |

Thickness is intumescent only.

Results also apply to I/H-section beams exposed on all four sides limited to a maximum protection thickness of 3.906mm.

Table 10: I/H-Column Sections 60 Minutes

| Section Factor up to m ⁻¹ | Thickness (mm) Required for a Design Temperature of | | | | | | | | |
|--------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|
| | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 650°C | 700°C | 750°C |
| 30 | 1.739 | 1.282 | 0.944 | 0.692 | 0.545 | 0.478 | 0.423 | 0.380 | 0.332 |
| 35 | 1.739 | 1.282 | 0.944 | 0.692 | 0.545 | 0.478 | 0.423 | 0.380 | 0.332 |
| 40 | 1.739 | 1.282 | 0.944 | 0.692 | 0.545 | 0.478 | 0.423 | 0.380 | 0.332 |
| 45 | 1.739 | 1.282 | 0.944 | 0.692 | 0.545 | 0.478 | 0.423 | 0.380 | 0.332 |
| 50 | 1.739 | 1.282 | 0.944 | 0.692 | 0.545 | 0.478 | 0.423 | 0.380 | 0.332 |
| 55 | 1.739 | 1.282 | 0.944 | 0.692 | 0.545 | 0.478 | 0.423 | 0.380 | 0.332 |
| 60 | 1.739 | 1.282 | 0.944 | 0.692 | 0.545 | 0.478 | 0.423 | 0.380 | 0.332 |
| 65 | 1.739 | 1.282 | 0.944 | 0.692 | 0.545 | 0.478 | 0.423 | 0.380 | 0.332 |
| 70 | 1.739 | 1.282 | 0.944 | 0.692 | 0.545 | 0.478 | 0.423 | 0.380 | 0.332 |
| 75 | 1.739 | 1.282 | 0.944 | 0.692 | 0.545 | 0.478 | 0.423 | 0.380 | 0.332 |
| 80 | 1.739 | 1.282 | 0.944 | 0.692 | 0.545 | 0.478 | 0.423 | 0.380 | 0.332 |
| 85 | 1.739 | 1.282 | 0.944 | 0.692 | 0.545 | 0.478 | 0.423 | 0.380 | 0.332 |
| 90 | 1.739 | 1.282 | 0.944 | 0.692 | 0.545 | 0.478 | 0.423 | 0.380 | 0.332 |
| 95 | 1.774 | 1.324 | 0.972 | 0.713 | 0.560 | 0.487 | 0.431 | 0.389 | 0.341 |
| 100 | 1.809 | 1.366 | 1.000 | 0.734 | 0.575 | 0.496 | 0.439 | 0.398 | 0.350 |
| 105 | 1.844 | 1.408 | 1.028 | 0.755 | 0.590 | 0.505 | 0.447 | 0.407 | 0.359 |
| 110 | 1.878 | 1.451 | 1.056 | 0.777 | 0.604 | 0.514 | 0.455 | 0.415 | 0.367 |
| 115 | 1.912 | 1.493 | 1.083 | 0.799 | 0.618 | 0.524 | 0.463 | 0.424 | 0.376 |
| 120 | 1.946 | 1.535 | 1.111 | 0.821 | 0.637 | 0.533 | 0.471 | 0.432 | 0.385 |
| 125 | 1.981 | 1.577 | 1.139 | 0.843 | 0.658 | 0.542 | 0.479 | 0.440 | 0.394 |
| 130 | 2.015 | 1.619 | 1.167 | 0.865 | 0.679 | 0.551 | 0.487 | 0.449 | 0.402 |
| 135 | 2.049 | 1.662 | 1.195 | 0.887 | 0.700 | 0.561 | 0.495 | 0.457 | 0.411 |
| 140 | 2.084 | 1.704 | 1.223 | 0.909 | 0.721 | 0.570 | 0.503 | 0.466 | 0.420 |
| 145 | 2.118 | 1.737 | 1.251 | 0.931 | 0.741 | 0.579 | 0.511 | 0.474 | 0.429 |
| 150 | 2.152 | 1.767 | 1.279 | 0.952 | 0.762 | 0.589 | 0.518 | 0.482 | 0.437 |
| 155 | 2.187 | 1.798 | 1.307 | 0.974 | 0.783 | 0.598 | 0.526 | 0.491 | 0.446 |
| 160 | 2.221 | 1.829 | 1.335 | 0.996 | 0.804 | 0.607 | 0.534 | 0.499 | 0.455 |
| 165 | 2.255 | 1.859 | 1.363 | 1.018 | 0.825 | 0.617 | 0.542 | 0.508 | 0.464 |
| 170 | 2.289 | 1.890 | 1.391 | 1.040 | 0.846 | 0.632 | 0.550 | 0.516 | 0.472 |
| 175 | 2.324 | 1.921 | 1.419 | 1.062 | 0.867 | 0.653 | 0.558 | 0.524 | 0.481 |
| 180 | 2.388 | 1.951 | 1.446 | 1.084 | 0.887 | 0.674 | 0.566 | 0.533 | 0.490 |
| 185 | 2.453 | 1.982 | 1.474 | 1.106 | 0.908 | 0.694 | 0.574 | 0.541 | 0.499 |
| 190 | 2.519 | 2.012 | 1.502 | 1.128 | 0.929 | 0.715 | 0.582 | 0.550 | 0.508 |
| 195 | 2.585 | 2.043 | 1.530 | 1.149 | 0.950 | 0.736 | 0.590 | 0.558 | 0.516 |
| 200 | 2.651 | 2.074 | 1.558 | 1.171 | 0.971 | 0.756 | 0.598 | 0.567 | 0.525 |
| 205 | 2.717 | 2.104 | 1.586 | 1.193 | 0.992 | 0.777 | 0.606 | 0.575 | 0.534 |
| 210 | 2.783 | 2.135 | 1.614 | 1.215 | 1.012 | 0.798 | 0.614 | 0.583 | 0.543 |
| 215 | 2.849 | 2.166 | 1.642 | 1.237 | 1.033 | 0.818 | 0.624 | 0.592 | 0.551 |
| 220 | 2.915 | 2.196 | 1.670 | 1.259 | 1.054 | 0.839 | 0.643 | 0.600 | 0.560 |
| 225 | 2.981 | 2.227 | 1.698 | 1.281 | 1.075 | 0.860 | 0.663 | 0.609 | 0.569 |
| 230 | 3.046 | 2.258 | 1.725 | 1.303 | 1.096 | 0.880 | 0.683 | 0.617 | 0.578 |
| 235 | 3.112 | 2.288 | 1.752 | 1.325 | 1.117 | 0.901 | 0.703 | 0.630 | 0.586 |
| 240 | 3.178 | 2.319 | 1.779 | 1.346 | 1.138 | 0.922 | 0.723 | 0.648 | 0.595 |
| 245 | 3.244 | 2.384 | 1.806 | 1.368 | 1.158 | 0.943 | 0.743 | 0.665 | 0.604 |
| 250 | 3.310 | 2.460 | 1.833 | 1.390 | 1.179 | 0.963 | 0.763 | 0.683 | 0.613 |
| 255 | 3.376 | 2.537 | 1.860 | 1.412 | 1.200 | 0.984 | 0.783 | 0.700 | 0.622 |
| 260 | 3.442 | 2.613 | 1.887 | 1.434 | 1.221 | 1.005 | 0.803 | 0.718 | 0.637 |
| 265 | 3.508 | 2.689 | 1.914 | 1.456 | 1.242 | 1.025 | 0.823 | 0.736 | 0.653 |
| 270 | 3.574 | 2.765 | 1.941 | 1.478 | 1.263 | 1.046 | 0.843 | 0.753 | 0.668 |
| 275 | 3.639 | 2.841 | 1.968 | 1.500 | 1.284 | 1.067 | 0.863 | 0.771 | 0.684 |
| 280 | 3.705 | 2.917 | 1.994 | 1.522 | 1.304 | 1.087 | 0.882 | 0.788 | 0.699 |
| 285 | 3.771 | 2.993 | 2.021 | 1.544 | 1.325 | 1.108 | 0.902 | 0.806 | 0.715 |
| 290 | 3.837 | 3.070 | 2.048 | 1.565 | 1.346 | 1.129 | 0.922 | 0.823 | 0.730 |
| 295 | 3.903 | 3.146 | 2.075 | 1.587 | 1.367 | 1.150 | 0.942 | 0.841 | 0.746 |
| 300 | 3.969 | 3.222 | 2.102 | 1.609 | 1.388 | 1.170 | 0.962 | 0.859 | 0.761 |
| 305 | 4.035 | 3.298 | 2.129 | 1.631 | 1.409 | 1.191 | 0.982 | 0.876 | 0.777 |
| 310 | 4.101 | 3.374 | 2.156 | 1.653 | 1.430 | 1.212 | 1.002 | 0.894 | 0.792 |
| 315 | 4.167 | 3.450 | 2.183 | 1.675 | 1.450 | 1.232 | 1.022 | 0.911 | 0.808 |
| 320 | 4.233 | 3.527 | 2.210 | 1.697 | 1.471 | 1.253 | 1.042 | 0.929 | 0.823 |
| 325 | 4.299 | 3.603 | 2.237 | 1.727 | 1.492 | 1.274 | 1.062 | 0.946 | 0.839 |
| 330 | 4.365 | 3.679 | 2.264 | 1.777 | 1.513 | 1.294 | 1.082 | 0.964 | 0.854 |
| 335 | 4.431 | 3.755 | 2.291 | 1.827 | 1.534 | 1.315 | 1.102 | 0.982 | 0.870 |
| 340 | 4.497 | 3.831 | 2.317 | 1.877 | 1.555 | 1.336 | 1.121 | 0.999 | 0.885 |
| 345 | 4.563 | 3.907 | 2.439 | 1.927 | 1.575 | 1.357 | 1.141 | 1.017 | 0.901 |
| 350 | 4.629 | 3.983 | 2.605 | 1.977 | 1.596 | 1.377 | 1.161 | 1.034 | 0.916 |
| 355 | - | 4.060 | 2.771 | 2.027 | 1.617 | 1.398 | 1.181 | 1.052 | 0.932 |
| 360 | - | 4.137 | 2.937 | 2.076 | 1.638 | 1.419 | 1.201 | 1.069 | 0.947 |
| 365 | - | 4.214 | 3.103 | 2.126 | 1.659 | 1.439 | 1.221 | 1.087 | 0.963 |

Thickness is intumescent only.

Results also apply to I/H-section beams exposed on all four sides limited to a maximum protection thickness of 3.906mm.

Table 11: I/H-Column Sections 75 Minutes

| Section Factor up to m ⁻¹ | Thickness (mm) Required for a Design Temperature of | | | | | | | | |
|--------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|
| | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 650°C | 700°C | 750°C |
| 30 | 2.127 | 1.768 | 1.372 | 1.081 | 0.853 | 0.676 | 0.574 | 0.531 | 0.485 |
| 35 | 2.127 | 1.768 | 1.372 | 1.081 | 0.853 | 0.676 | 0.574 | 0.531 | 0.485 |
| 40 | 2.127 | 1.768 | 1.372 | 1.081 | 0.853 | 0.676 | 0.574 | 0.531 | 0.485 |
| 45 | 2.127 | 1.768 | 1.372 | 1.081 | 0.853 | 0.676 | 0.574 | 0.531 | 0.485 |
| 50 | 2.127 | 1.768 | 1.372 | 1.081 | 0.853 | 0.676 | 0.574 | 0.531 | 0.485 |
| 55 | 2.127 | 1.768 | 1.372 | 1.081 | 0.853 | 0.676 | 0.574 | 0.531 | 0.485 |
| 60 | 2.127 | 1.768 | 1.372 | 1.081 | 0.853 | 0.676 | 0.574 | 0.531 | 0.485 |
| 65 | 2.127 | 1.768 | 1.372 | 1.081 | 0.853 | 0.676 | 0.574 | 0.531 | 0.485 |
| 70 | 2.127 | 1.768 | 1.372 | 1.081 | 0.853 | 0.676 | 0.574 | 0.531 | 0.485 |
| 75 | 2.127 | 1.768 | 1.372 | 1.081 | 0.853 | 0.676 | 0.574 | 0.531 | 0.485 |
| 80 | 2.127 | 1.768 | 1.372 | 1.081 | 0.853 | 0.676 | 0.574 | 0.531 | 0.485 |
| 85 | 2.127 | 1.768 | 1.372 | 1.081 | 0.853 | 0.676 | 0.574 | 0.531 | 0.485 |
| 90 | 2.127 | 1.768 | 1.372 | 1.081 | 0.853 | 0.676 | 0.574 | 0.531 | 0.485 |
| 95 | 2.182 | 1.808 | 1.425 | 1.119 | 0.880 | 0.697 | 0.589 | 0.543 | 0.495 |
| 100 | 2.237 | 1.848 | 1.478 | 1.157 | 0.907 | 0.718 | 0.604 | 0.555 | 0.505 |
| 105 | 2.292 | 1.888 | 1.531 | 1.195 | 0.934 | 0.739 | 0.619 | 0.567 | 0.515 |
| 110 | 2.347 | 1.928 | 1.583 | 1.234 | 0.961 | 0.760 | 0.638 | 0.579 | 0.525 |
| 115 | 2.402 | 1.968 | 1.635 | 1.272 | 0.987 | 0.781 | 0.658 | 0.591 | 0.535 |
| 120 | 2.457 | 2.007 | 1.688 | 1.310 | 1.014 | 0.802 | 0.678 | 0.602 | 0.544 |
| 125 | 2.512 | 2.047 | 1.731 | 1.349 | 1.041 | 0.823 | 0.698 | 0.614 | 0.554 |
| 130 | 2.567 | 2.087 | 1.767 | 1.387 | 1.067 | 0.843 | 0.718 | 0.629 | 0.564 |
| 135 | 2.622 | 2.127 | 1.802 | 1.425 | 1.094 | 0.864 | 0.738 | 0.648 | 0.574 |
| 140 | 2.677 | 2.167 | 1.838 | 1.464 | 1.121 | 0.885 | 0.758 | 0.667 | 0.584 |
| 145 | 2.732 | 2.207 | 1.873 | 1.502 | 1.148 | 0.906 | 0.778 | 0.686 | 0.594 |
| 150 | 2.787 | 2.247 | 1.909 | 1.540 | 1.174 | 0.927 | 0.798 | 0.705 | 0.604 |
| 155 | 2.842 | 2.287 | 1.945 | 1.579 | 1.201 | 0.948 | 0.818 | 0.724 | 0.614 |
| 160 | 2.897 | 2.329 | 1.980 | 1.617 | 1.228 | 0.969 | 0.838 | 0.743 | 0.626 |
| 165 | 2.952 | 2.425 | 2.016 | 1.655 | 1.254 | 0.990 | 0.858 | 0.762 | 0.645 |
| 170 | 3.007 | 2.521 | 2.051 | 1.694 | 1.281 | 1.011 | 0.878 | 0.781 | 0.663 |
| 175 | 3.062 | 2.617 | 2.087 | 1.730 | 1.308 | 1.032 | 0.898 | 0.800 | 0.682 |
| 180 | 3.117 | 2.713 | 2.123 | 1.765 | 1.335 | 1.053 | 0.918 | 0.819 | 0.700 |
| 185 | 3.172 | 2.809 | 2.158 | 1.800 | 1.361 | 1.074 | 0.938 | 0.839 | 0.719 |
| 190 | 3.227 | 2.905 | 2.194 | 1.835 | 1.388 | 1.095 | 0.958 | 0.858 | 0.737 |
| 195 | 3.282 | 3.001 | 2.229 | 1.869 | 1.415 | 1.116 | 0.978 | 0.877 | 0.756 |
| 200 | 3.337 | 3.097 | 2.265 | 1.904 | 1.441 | 1.136 | 0.998 | 0.896 | 0.775 |
| 205 | 3.392 | 3.193 | 2.300 | 1.939 | 1.468 | 1.157 | 1.018 | 0.915 | 0.793 |
| 210 | 3.447 | 3.289 | 2.350 | 1.974 | 1.495 | 1.178 | 1.038 | 0.934 | 0.812 |
| 215 | 3.502 | 3.385 | 2.434 | 2.008 | 1.522 | 1.199 | 1.058 | 0.953 | 0.830 |
| 220 | 3.557 | 3.481 | 2.517 | 2.043 | 1.548 | 1.220 | 1.078 | 0.972 | 0.849 |
| 225 | 3.612 | 3.577 | 2.601 | 2.078 | 1.575 | 1.241 | 1.098 | 0.991 | 0.868 |
| 230 | 3.674 | 3.674 | 2.685 | 2.113 | 1.602 | 1.262 | 1.118 | 1.010 | 0.886 |
| 235 | 3.770 | 3.770 | 2.769 | 2.147 | 1.628 | 1.283 | 1.138 | 1.029 | 0.905 |
| 240 | 3.866 | 3.866 | 2.853 | 2.182 | 1.655 | 1.304 | 1.158 | 1.048 | 0.923 |
| 245 | 3.962 | 3.962 | 2.937 | 2.217 | 1.682 | 1.325 | 1.178 | 1.067 | 0.942 |
| 250 | 4.058 | 4.058 | 3.021 | 2.252 | 1.708 | 1.346 | 1.198 | 1.086 | 0.961 |
| 255 | 4.154 | 4.154 | 3.105 | 2.286 | 1.742 | 1.367 | 1.218 | 1.105 | 0.979 |
| 260 | 4.250 | 4.250 | 3.189 | 2.321 | 1.776 | 1.388 | 1.238 | 1.124 | 0.998 |
| 265 | 4.346 | 4.346 | 3.273 | 2.422 | 1.810 | 1.409 | 1.258 | 1.143 | 1.016 |
| 270 | 4.442 | 4.442 | 3.357 | 2.534 | 1.845 | 1.430 | 1.278 | 1.162 | 1.035 |
| 275 | 4.538 | 4.538 | 3.440 | 2.645 | 1.879 | 1.450 | 1.298 | 1.181 | 1.054 |
| 280 | 4.634 | 4.634 | 3.524 | 2.757 | 1.913 | 1.471 | 1.318 | 1.200 | 1.072 |
| 285 | - | - | 3.608 | 2.869 | 1.947 | 1.492 | 1.338 | 1.219 | 1.091 |
| 290 | - | - | 3.692 | 2.980 | 1.982 | 1.513 | 1.358 | 1.238 | 1.109 |
| 295 | - | - | 3.776 | 3.092 | 2.016 | 1.534 | 1.378 | 1.257 | 1.128 |
| 300 | - | - | 3.860 | 3.204 | 2.050 | 1.555 | 1.398 | 1.276 | 1.147 |
| 305 | - | - | 3.944 | 3.315 | 2.085 | 1.576 | 1.418 | 1.295 | 1.165 |
| 310 | - | - | 4.028 | 3.427 | 2.119 | 1.597 | 1.438 | 1.314 | 1.184 |
| 315 | - | - | 4.112 | 3.538 | 2.153 | 1.618 | 1.458 | 1.333 | 1.202 |
| 320 | - | - | 4.196 | 3.650 | 2.187 | 1.639 | 1.478 | 1.352 | 1.221 |
| 325 | - | - | 4.280 | 3.762 | 2.222 | 1.660 | 1.498 | 1.371 | 1.239 |
| 330 | - | - | 4.364 | 3.873 | 2.256 | 1.681 | 1.518 | 1.390 | 1.258 |
| 335 | - | - | 4.448 | 3.985 | 2.290 | 1.702 | 1.538 | 1.409 | 1.277 |
| 340 | - | - | 4.532 | 4.097 | 2.324 | 1.750 | 1.558 | 1.428 | 1.295 |
| 345 | - | - | 4.616 | 4.209 | 2.628 | 1.825 | 1.578 | 1.447 | 1.314 |
| 350 | - | - | - | 4.321 | 2.945 | 1.899 | 1.598 | 1.466 | 1.332 |
| 355 | - | - | - | 4.433 | 3.262 | 1.974 | 1.618 | 1.485 | 1.351 |
| 360 | - | - | - | 4.545 | 3.578 | 2.049 | 1.638 | 1.504 | 1.370 |
| 365 | - | - | - | - | 3.895 | 2.124 | 1.658 | 1.523 | 1.388 |

Thickness is intumescent only.

Results also apply to I/H-section beams exposed on all four sides limited to a maximum protection thickness of 3.906mm.

Table 12: I/H-Column Sections 90 Minutes

| Section Factor up to m ⁻¹ | Thickness (mm) Required for a Design Temperature of | | | | | | | | |
|--------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|
| | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 650°C | 700°C | 750°C |
| 30 | - | 2.131 | 1.804 | 1.469 | 1.202 | 0.994 | 0.837 | 0.739 | 0.654 |
| 35 | - | 2.131 | 1.804 | 1.469 | 1.202 | 0.994 | 0.837 | 0.739 | 0.654 |
| 40 | - | 2.131 | 1.804 | 1.469 | 1.202 | 0.994 | 0.837 | 0.739 | 0.654 |
| 45 | - | 2.131 | 1.804 | 1.469 | 1.202 | 0.994 | 0.837 | 0.739 | 0.654 |
| 50 | - | 2.131 | 1.804 | 1.469 | 1.202 | 0.994 | 0.837 | 0.739 | 0.654 |
| 55 | - | 2.131 | 1.804 | 1.469 | 1.202 | 0.994 | 0.837 | 0.739 | 0.654 |
| 60 | - | 2.131 | 1.804 | 1.469 | 1.202 | 0.994 | 0.837 | 0.739 | 0.654 |
| 65 | - | 2.131 | 1.804 | 1.469 | 1.202 | 0.994 | 0.837 | 0.739 | 0.654 |
| 70 | - | 2.131 | 1.804 | 1.469 | 1.202 | 0.994 | 0.837 | 0.739 | 0.654 |
| 75 | - | 2.131 | 1.804 | 1.469 | 1.202 | 0.994 | 0.837 | 0.739 | 0.654 |
| 80 | - | 2.131 | 1.804 | 1.469 | 1.202 | 0.994 | 0.837 | 0.739 | 0.654 |
| 85 | - | 2.131 | 1.804 | 1.469 | 1.202 | 0.994 | 0.837 | 0.739 | 0.654 |
| 90 | - | 2.131 | 1.804 | 1.469 | 1.202 | 0.994 | 0.837 | 0.739 | 0.654 |
| 95 | - | 2.191 | 1.852 | 1.529 | 1.248 | 1.027 | 0.861 | 0.759 | 0.673 |
| 100 | - | 2.252 | 1.900 | 1.589 | 1.294 | 1.060 | 0.885 | 0.779 | 0.692 |
| 105 | - | 2.312 | 1.948 | 1.649 | 1.340 | 1.093 | 0.909 | 0.799 | 0.711 |
| 110 | - | 2.372 | 1.997 | 1.710 | 1.387 | 1.127 | 0.934 | 0.819 | 0.731 |
| 115 | - | 2.432 | 2.045 | 1.751 | 1.433 | 1.161 | 0.958 | 0.839 | 0.751 |
| 120 | - | 2.492 | 2.094 | 1.791 | 1.479 | 1.195 | 0.982 | 0.859 | 0.770 |
| 125 | - | 2.553 | 2.143 | 1.832 | 1.526 | 1.229 | 1.007 | 0.879 | 0.790 |
| 130 | - | 2.613 | 2.191 | 1.872 | 1.572 | 1.263 | 1.031 | 0.898 | 0.809 |
| 135 | - | 2.673 | 2.240 | 1.912 | 1.619 | 1.296 | 1.055 | 0.918 | 0.829 |
| 140 | - | 2.733 | 2.288 | 1.953 | 1.665 | 1.330 | 1.079 | 0.938 | 0.849 |
| 145 | - | 2.794 | 2.382 | 1.993 | 1.711 | 1.364 | 1.104 | 0.958 | 0.868 |
| 150 | - | 2.854 | 2.636 | 2.034 | 1.749 | 1.398 | 1.128 | 0.978 | 0.888 |
| 155 | - | 2.914 | 2.890 | 2.074 | 1.786 | 1.432 | 1.152 | 0.997 | 0.907 |
| 160 | - | 3.143 | 3.143 | 2.115 | 1.823 | 1.466 | 1.176 | 1.017 | 0.927 |
| 165 | - | 3.397 | 3.397 | 2.155 | 1.861 | 1.499 | 1.201 | 1.037 | 0.947 |
| 170 | - | 3.650 | 3.650 | 2.195 | 1.898 | 1.533 | 1.225 | 1.057 | 0.966 |
| 175 | - | 3.904 | 3.904 | 2.236 | 1.935 | 1.567 | 1.249 | 1.077 | 0.986 |
| 180 | - | 4.158 | 4.158 | 2.276 | 1.973 | 1.601 | 1.274 | 1.096 | 1.005 |
| 185 | - | 4.412 | 4.412 | 2.317 | 2.010 | 1.635 | 1.298 | 1.116 | 1.025 |
| 190 | - | - | - | 2.450 | 2.048 | 1.669 | 1.322 | 1.136 | 1.045 |
| 195 | - | - | - | 2.613 | 2.085 | 1.702 | 1.346 | 1.156 | 1.064 |
| 200 | - | - | - | 2.775 | 2.122 | 1.737 | 1.371 | 1.176 | 1.084 |
| 205 | - | - | - | 2.937 | 2.160 | 1.772 | 1.395 | 1.195 | 1.103 |
| 210 | - | - | - | 3.100 | 2.197 | 1.806 | 1.419 | 1.215 | 1.123 |
| 215 | - | - | - | 3.262 | 2.234 | 1.841 | 1.444 | 1.235 | 1.143 |
| 220 | - | - | - | 3.424 | 2.272 | 1.876 | 1.468 | 1.255 | 1.162 |
| 225 | - | - | - | 3.586 | 2.309 | 1.911 | 1.492 | 1.275 | 1.182 |
| 230 | - | - | - | 3.749 | 2.388 | 1.945 | 1.516 | 1.295 | 1.201 |
| 235 | - | - | - | 3.911 | 2.504 | 1.980 | 1.541 | 1.314 | 1.221 |
| 240 | - | - | - | 4.073 | 2.619 | 2.015 | 1.565 | 1.334 | 1.240 |
| 245 | - | - | - | 4.235 | 2.734 | 2.050 | 1.589 | 1.354 | 1.260 |
| 250 | - | - | - | 4.397 | 2.849 | 2.084 | 1.613 | 1.374 | 1.280 |
| 255 | - | - | - | 4.559 | 2.964 | 2.119 | 1.638 | 1.394 | 1.299 |
| 260 | - | - | - | - | 3.080 | 2.154 | 1.662 | 1.413 | 1.319 |
| 265 | - | - | - | - | 3.195 | 2.189 | 1.686 | 1.433 | 1.338 |
| 270 | - | - | - | - | 3.310 | 2.223 | 1.711 | 1.453 | 1.358 |
| 275 | - | - | - | - | 3.425 | 2.258 | 1.752 | 1.473 | 1.378 |
| 280 | - | - | - | - | 3.540 | 2.293 | 1.795 | 1.493 | 1.397 |
| 285 | - | - | - | - | 3.655 | 2.335 | 1.837 | 1.512 | 1.417 |
| 290 | - | - | - | - | 3.771 | 2.534 | 1.880 | 1.532 | 1.436 |
| 295 | - | - | - | - | 3.886 | 2.733 | 1.923 | 1.552 | 1.456 |
| 300 | - | - | - | - | 4.001 | 2.932 | 1.965 | 1.572 | 1.476 |
| 305 | - | - | - | - | 4.116 | 3.131 | 2.008 | 1.592 | 1.495 |
| 310 | - | - | - | - | 4.231 | 3.330 | 2.051 | 1.611 | 1.515 |
| 315 | - | - | - | - | 4.346 | 3.529 | 2.093 | 1.631 | 1.534 |
| 320 | - | - | - | - | 4.461 | 3.728 | 2.136 | 1.651 | 1.554 |
| 325 | - | - | - | - | 4.576 | 3.927 | 2.179 | 1.671 | 1.574 |
| 330 | - | - | - | - | - | 4.126 | 2.221 | 1.691 | 1.593 |
| 335 | - | - | - | - | - | 4.325 | 2.264 | 1.711 | 1.613 |
| 340 | - | - | - | - | - | 4.524 | 2.307 | 1.805 | 1.632 |
| 345 | - | - | - | - | - | - | 2.689 | 1.905 | 1.652 |
| 350 | - | - | - | - | - | - | 3.354 | 2.005 | 1.672 |
| 355 | - | - | - | - | - | - | 4.018 | 2.105 | 1.691 |
| 360 | - | - | - | - | - | - | - | 2.205 | 1.711 |
| 365 | - | - | - | - | - | - | - | 2.306 | 1.814 |

Thickness is intumescent only.

Results also apply to I/H-section beams exposed on all four sides limited to a maximum protection thickness of 3.906mm.

Table 13: I/H-Column Sections 105 Minutes

| Section Factor up to m ⁻¹ | Thickness (mm) Required for a Design Temperature of | | | | | | | | |
|--------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|
| | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 650°C | 700°C | 750°C |
| 30 | - | - | 2.151 | 1.854 | 1.552 | 1.305 | 1.113 | 1.002 | 0.916 |
| 35 | - | - | 2.151 | 1.854 | 1.552 | 1.305 | 1.113 | 1.002 | 0.916 |
| 40 | - | - | 2.151 | 1.854 | 1.552 | 1.305 | 1.113 | 1.002 | 0.916 |
| 45 | - | - | 2.151 | 1.854 | 1.552 | 1.305 | 1.113 | 1.002 | 0.916 |
| 50 | - | - | 2.151 | 1.854 | 1.552 | 1.305 | 1.113 | 1.002 | 0.916 |
| 55 | - | - | 2.151 | 1.854 | 1.552 | 1.305 | 1.113 | 1.002 | 0.916 |
| 60 | - | - | 2.151 | 1.854 | 1.552 | 1.305 | 1.113 | 1.002 | 0.916 |
| 65 | - | - | 2.151 | 1.854 | 1.552 | 1.305 | 1.113 | 1.002 | 0.916 |
| 70 | - | - | 2.151 | 1.854 | 1.552 | 1.305 | 1.113 | 1.002 | 0.916 |
| 75 | - | - | 2.151 | 1.854 | 1.552 | 1.305 | 1.113 | 1.002 | 0.916 |
| 80 | - | - | 2.151 | 1.854 | 1.552 | 1.305 | 1.113 | 1.002 | 0.916 |
| 85 | - | - | 2.151 | 1.854 | 1.552 | 1.305 | 1.113 | 1.002 | 0.916 |
| 90 | - | - | 2.151 | 1.854 | 1.552 | 1.305 | 1.113 | 1.002 | 0.916 |
| 95 | - | - | 2.219 | 1.911 | 1.618 | 1.356 | 1.153 | 1.033 | 0.942 |
| 100 | - | - | 2.287 | 1.968 | 1.685 | 1.407 | 1.193 | 1.064 | 0.968 |
| 105 | - | - | 2.354 | 2.025 | 1.738 | 1.458 | 1.233 | 1.095 | 0.994 |
| 110 | - | - | 2.422 | 2.083 | 1.784 | 1.510 | 1.272 | 1.127 | 1.020 |
| 115 | - | - | 2.490 | 2.140 | 1.829 | 1.561 | 1.312 | 1.159 | 1.046 |
| 120 | - | - | 2.558 | 2.198 | 1.874 | 1.613 | 1.351 | 1.190 | 1.072 |
| 125 | - | - | 2.625 | 2.255 | 1.919 | 1.664 | 1.391 | 1.222 | 1.098 |
| 130 | - | - | 2.693 | 2.313 | 1.965 | 1.715 | 1.430 | 1.253 | 1.124 |
| 135 | - | - | 2.761 | 2.371 | 2.010 | 1.755 | 1.470 | 1.285 | 1.150 |
| 140 | - | - | 2.829 | 2.429 | 2.055 | 1.796 | 1.509 | 1.317 | 1.176 |
| 145 | - | - | 2.896 | 2.487 | 2.100 | 1.836 | 1.549 | 1.348 | 1.202 |
| 150 | - | - | 2.964 | 2.545 | 2.146 | 1.877 | 1.588 | 1.380 | 1.228 |
| 155 | - | - | 3.032 | 2.603 | 2.191 | 1.917 | 1.628 | 1.411 | 1.254 |
| 160 | - | - | 3.100 | 2.661 | 2.236 | 1.957 | 1.667 | 1.443 | 1.280 |
| 165 | - | - | 3.168 | 2.719 | 2.281 | 1.998 | 1.707 | 1.474 | 1.306 |
| 170 | - | - | 3.235 | 2.777 | 2.345 | 2.038 | 1.745 | 1.506 | 1.332 |
| 175 | - | - | 4.066 | 4.066 | 4.066 | 2.079 | 1.783 | 1.538 | 1.358 |
| 180 | - | - | - | - | - | 2.119 | 1.821 | 1.569 | 1.384 |
| 185 | - | - | - | - | - | 2.160 | 1.859 | 1.601 | 1.410 |
| 190 | - | - | - | - | - | 2.200 | 1.896 | 1.632 | 1.436 |
| 195 | - | - | - | - | - | 2.240 | 1.934 | 1.664 | 1.462 |
| 200 | - | - | - | - | - | 2.281 | 1.972 | 1.696 | 1.488 |
| 205 | - | - | - | - | - | 2.321 | 2.010 | 1.730 | 1.515 |
| 210 | - | - | - | - | - | 2.619 | 2.048 | 1.768 | 1.541 |
| 215 | - | - | - | - | - | 2.951 | 2.086 | 1.806 | 1.567 |
| 220 | - | - | - | - | - | 3.282 | 2.124 | 1.844 | 1.593 |
| 225 | - | - | - | - | - | 3.614 | 2.162 | 1.882 | 1.619 |
| 230 | - | - | - | - | - | 3.945 | 2.200 | 1.920 | 1.645 |
| 235 | - | - | - | - | - | 4.276 | 2.238 | 1.958 | 1.671 |
| 240 | - | - | - | - | - | 4.607 | 2.275 | 1.996 | 1.697 |
| 245 | - | - | - | - | - | - | 2.313 | 2.034 | 1.731 |
| 250 | - | - | - | - | - | - | 2.435 | 2.072 | 1.776 |
| 255 | - | - | - | - | - | - | 2.599 | 2.110 | 1.821 |
| 260 | - | - | - | - | - | - | 2.763 | 2.149 | 1.866 |
| 265 | - | - | - | - | - | - | 2.927 | 2.187 | 1.911 |
| 270 | - | - | - | - | - | - | 3.091 | 2.225 | 1.956 |
| 275 | - | - | - | - | - | - | 3.254 | 2.263 | 2.001 |
| 280 | - | - | - | - | - | - | 3.418 | 2.301 | 2.046 |
| 285 | - | - | - | - | - | - | 3.582 | 2.410 | 2.091 |
| 290 | - | - | - | - | - | - | 3.746 | 2.663 | 2.136 |
| 295 | - | - | - | - | - | - | 3.910 | 2.916 | 2.182 |
| 300 | - | - | - | - | - | - | 4.074 | 3.170 | 2.227 |
| 305 | - | - | - | - | - | - | 4.238 | 3.423 | 2.272 |
| 310 | - | - | - | - | - | - | 4.402 | 3.676 | 2.317 |
| 315 | - | - | - | - | - | - | 4.566 | 3.929 | 2.652 |
| 320 | - | - | - | - | - | - | - | 4.182 | 3.061 |
| 325 | - | - | - | - | - | - | - | 4.435 | 3.470 |
| 330 | - | - | - | - | - | - | - | - | 3.879 |
| 335 | - | - | - | - | - | - | - | - | 4.288 |
| 340 | - | - | - | - | - | - | - | - | - |
| 345 | - | - | - | - | - | - | - | - | - |
| 350 | - | - | - | - | - | - | - | - | - |
| 355 | - | - | - | - | - | - | - | - | - |
| 360 | - | - | - | - | - | - | - | - | - |
| 365 | - | - | - | - | - | - | - | - | - |

Thickness is intumescent only.

Results also apply to I/H-section beams exposed on all four sides limited to a maximum protection thickness of 3.906mm.

Table 14: I/H-Column Sections 120 Minutes

| Section Factor up to m ⁻¹ | Thickness (mm) Required for a Design Temperature of | | | | | | | | |
|--------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|
| | 350°C | 400°C | 450°C | 500°C | 550°C | 600°C | 650°C | 700°C | 750°C |
| 30 | - | - | - | 2.190 | 1.897 | 1.637 | 1.391 | 1.259 | 1.172 |
| 35 | - | - | - | 2.190 | 1.897 | 1.637 | 1.391 | 1.259 | 1.172 |
| 40 | - | - | - | 2.190 | 1.897 | 1.637 | 1.391 | 1.259 | 1.172 |
| 45 | - | - | - | 2.190 | 1.897 | 1.637 | 1.391 | 1.259 | 1.172 |
| 50 | - | - | - | 2.190 | 1.897 | 1.637 | 1.391 | 1.259 | 1.172 |
| 55 | - | - | - | 2.190 | 1.897 | 1.637 | 1.391 | 1.259 | 1.172 |
| 60 | - | - | - | 2.190 | 1.897 | 1.637 | 1.391 | 1.259 | 1.172 |
| 65 | - | - | - | 2.190 | 1.897 | 1.637 | 1.391 | 1.259 | 1.172 |
| 70 | - | - | - | 2.190 | 1.897 | 1.637 | 1.391 | 1.259 | 1.172 |
| 75 | - | - | - | 2.190 | 1.897 | 1.637 | 1.391 | 1.259 | 1.172 |
| 80 | - | - | - | 2.190 | 1.897 | 1.637 | 1.391 | 1.259 | 1.172 |
| 85 | - | - | - | 2.190 | 1.897 | 1.637 | 1.391 | 1.259 | 1.172 |
| 90 | - | - | - | 2.190 | 1.897 | 1.637 | 1.391 | 1.259 | 1.172 |
| 95 | - | - | - | 2.266 | 1.962 | 1.692 | 1.447 | 1.306 | 1.212 |
| 100 | - | - | - | 2.343 | 2.027 | 1.747 | 1.503 | 1.353 | 1.252 |
| 105 | - | - | - | 2.419 | 2.092 | 1.800 | 1.559 | 1.400 | 1.292 |
| 110 | - | - | - | 2.496 | 2.156 | 1.854 | 1.614 | 1.446 | 1.332 |
| 115 | - | - | - | 2.572 | 2.220 | 1.907 | 1.670 | 1.492 | 1.373 |
| 120 | - | - | - | 2.649 | 2.284 | 1.961 | 1.722 | 1.539 | 1.413 |
| 125 | - | - | - | 2.725 | 2.348 | 2.014 | 1.767 | 1.585 | 1.454 |
| 130 | - | - | - | 2.802 | 2.412 | 2.068 | 1.812 | 1.631 | 1.494 |
| 135 | - | - | - | 2.878 | 2.476 | 2.121 | 1.857 | 1.677 | 1.535 |
| 140 | - | - | - | 2.955 | 2.540 | 2.175 | 1.901 | 1.758 | 1.575 |
| 145 | - | - | - | 3.031 | 2.604 | 2.228 | 1.946 | 1.940 | 1.615 |
| 150 | - | - | - | 3.108 | 2.668 | 2.281 | 2.122 | 2.122 | 1.656 |
| 155 | - | - | - | 3.184 | 2.732 | 2.334 | 2.304 | 2.304 | 1.696 |
| 160 | - | - | - | 3.261 | 2.796 | 2.486 | 2.486 | 2.486 | 1.738 |
| 165 | - | - | - | 3.337 | 2.860 | 2.668 | 2.668 | 2.668 | 1.781 |
| 170 | - | - | - | 3.414 | 2.924 | 2.850 | 2.850 | 2.850 | 1.824 |
| 175 | - | - | - | 3.490 | 3.032 | 3.032 | 3.032 | 3.032 | 1.866 |
| 180 | - | - | - | 3.567 | 3.214 | 3.214 | 3.214 | 3.214 | 1.909 |
| 185 | - | - | - | 3.643 | 3.396 | 3.396 | 3.396 | 3.396 | 1.952 |
| 190 | - | - | - | 3.720 | 3.578 | 3.578 | 3.578 | 3.578 | 1.995 |
| 195 | - | - | - | 3.796 | 3.760 | 3.760 | 3.760 | 3.760 | 2.037 |
| 200 | - | - | - | 3.943 | 3.943 | 3.943 | 3.943 | 3.943 | 2.080 |
| 205 | - | - | - | 4.125 | 4.125 | 4.125 | 4.125 | 4.125 | 2.123 |
| 210 | - | - | - | 4.307 | 4.307 | 4.307 | 4.307 | 4.307 | 2.166 |
| 215 | - | - | - | 4.489 | 4.489 | 4.489 | 4.489 | 4.489 | 2.208 |
| 220 | - | - | - | - | - | - | - | - | 2.251 |
| 225 | - | - | - | - | - | - | - | - | 2.294 |
| 230 | - | - | - | - | - | - | - | - | 2.685 |
| 235 | - | - | - | - | - | - | - | - | 4.116 |
| 240 | - | - | - | - | - | - | - | - | - |
| 245 | - | - | - | - | - | - | - | - | - |
| 250 | - | - | - | - | - | - | - | - | - |
| 255 | - | - | - | - | - | - | - | - | - |
| 260 | - | - | - | - | - | - | - | - | - |
| 265 | - | - | - | - | - | - | - | - | - |
| 270 | - | - | - | - | - | - | - | - | - |
| 275 | - | - | - | - | - | - | - | - | - |
| 280 | - | - | - | - | - | - | - | - | - |
| 285 | - | - | - | - | - | - | - | - | - |
| 290 | - | - | - | - | - | - | - | - | - |
| 295 | - | - | - | - | - | - | - | - | - |
| 300 | - | - | - | - | - | - | - | - | - |
| 305 | - | - | - | - | - | - | - | - | - |
| 310 | - | - | - | - | - | - | - | - | - |
| 315 | - | - | - | - | - | - | - | - | - |
| 320 | - | - | - | - | - | - | - | - | - |
| 325 | - | - | - | - | - | - | - | - | - |
| 330 | - | - | - | - | - | - | - | - | - |
| 335 | - | - | - | - | - | - | - | - | - |
| 340 | - | - | - | - | - | - | - | - | - |
| 345 | - | - | - | - | - | - | - | - | - |
| 350 | - | - | - | - | - | - | - | - | - |
| 355 | - | - | - | - | - | - | - | - | - |
| 360 | - | - | - | - | - | - | - | - | - |
| 365 | - | - | - | - | - | - | - | - | - |

Thickness is intumescent only.

Results also apply to I/H-section beams exposed on all four sides limited to a maximum protection thickness of 3.906mm.